APPENDIX O

STORM WATER MANAGEMENT REPORT







Spadina Subway Extension – Downsview Station to Steeles Avenue Environmental Assessment





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CHAPTER 1.0 INTRODUCTION AND DESIGN STANDARDS

1.1 STUDY PURPOSE

As part of the Spadina Subway Extension Environmental Assessment, the construction of four (4) subway stations and affiliated parking is proposed. Table 1.1 identifies new impervious areas associated with these facilities. A plan showing the locations of these proposed subway stations is provided in Exhibit 1.1.

Table 1.1 - Proposed Subway Station Descriptions

| Location | Proposed Facility | New Impervious Area (ha) |
|-------------------------|---|--------------------------|
| Sheppard Avenue West | Station Building | 0.2 |
| Finch West | Commuter Parking Lot | 2.3 |
| | Passenger Pick-Up/Drop-Off | 0.3 |
| | Bus Terminal / Roads / Station Building | 1.2 |
| York University Station | Station Building | 0.1 |
| Steeles West Station | East Commuter Parking Lot | 5.2 |
| | West Commuter Parking Lot | 4.9 |
| | Inter-Regional Bus Terminal (north of Steeles) / Station Building | 2.1 |

The proposed subway extension alignment generally follows the divide between the Black Creek subwatershed and the Lower West Don River subwatershed within the Humber Watershed. As a result, surface water is generally conveyed away from each of the proposed station locations to an outlet to one of the two aforementioned watercourses via the existing sewer networks.

With the exception of the Finch West and Steeles West stations where commuter parking lots and bus terminals are proposed, increases in impervious areas resulting from the undertaking consist mainly of small entrance / exit buildings. New roads are proposed at the Steeles West Station but are addressed as part of York Region's Highway 7 Transitway Environmental Assessment. The proposed GO Transit platform at the Sheppard West Station will be addressed under a separate GO Transit Environmental Assessment.

The placement of these permanent facilities with impervious areas may affect the drainage characteristics and quality of runoff from the affected subwatersheds. To offset these potential impacts, lot level conveyance and quality controls will be implemented. To address these potential changes in hydraulic performance, a stormwater management plan for each proposed site has been prepared and is discussed below.

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Exhibit 1.1 - Proposed Subway Station Locations



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1.2 STUDY SCOPE

This stormwater management (SWM) report includes the following for each proposed station location:

- Identification of the existing drainage condition;
- Proposed Drainage Condition; and
- Stormwater Management Plan (Water Quality and Quantity Control, Water Balance, and Erosion and Sediment Control requirements).

In addition, it is assumed that stormwater management of all underground facilities will be conducted in accordance with standard building code practice with connections to sanitary sewers. For above ground facilities, (stations and transit facilities including bus terminals, commuter parking lots and passenger drop-off / pick-up facilities), downspouts will outlet at ground level. In the case of substations without roofs, it is assumed that their floor drains will also outlet at ground level.

1.3 STORMWATER MANAGEMENT DESIGN CRITERIA - CITY OF TORONTO

In accordance with the City of Toronto's Wet Weather Flow Management Policy (August 2003), the following (interim) must be addressed during design for all proposed subway stations:

- Water Quality; •
- Water Quantity including erosion control and; and
- Water Balance.

1.3.1 Water Quality - Total Suspended Solids (TSS)

The wet weather flow (WWF) water quality target is the long-term average removal of 80% of the Total Suspended Solids (TSS) on annual loading basis from all runoff leaving the development site based on the post-development level of imperviousness.

1.3.2 Water Quantity

a) Flood Flow Management Criteria

The required level of peak flow control from the development site shall follow Toronto and Region Conservation Authority (TRCA) Flood Flow Criteria Map, which indicates that quantity control should ensure post to pre-development peak flows for 2 to 100-year return period events. For redevelopment sites < 5 ha, peak flows can be computed using simplified approach such as the Rational Method and IDF curves. Refer to Appendix A for a copy of TRCA's Flood Flow Criteria Map.

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b) Erosion Control

The TTC must contact TRCA staff to determine erosion control/geomorphology requirements for individual development sites in the planning stage (TRCA's response has been noted in each section addressing erosion and sediment control).

- 1. For Rouge River watershed, follow TRCA (Toronto Region Conservation Authority) erosion control criteria for individual sites, which discharge directly to and/or are in proximity of natural watercourses;
- 2. For all new large development blocks, which discharge directly to and/or in proximity of natural watercourses within other watersheds, the proponents are required to complete an Erosion Analysis Report to determine the erosion control criteria for the sites. Please consult TRCA for further details.
- 3. For new development blocks where it is not feasible (i.e. proposed development is negligible with respect to the total drainage area of the receiving watercourse) to complete an Erosion Analysis Report, TRCA typically requires that runoff from a 25 mm storm shall be detained on-site and released over a minimum of 24 hours.
- 4. For small infill/redevelopment sites < 2 ha, erosion control in the form of stormwater detention is normally not required, provided the on-site minimum runoff retention from a 5 mm daily rainfall event is achieved under the Water Balance Criteria.

c) Erosion and Sediment Control During Construction

The City of Toronto Erosion Control Criteria during construction are as follows:

- · Regardless of size for all development sites, temporary erosion and sediment control for construction must be provided on-site.
- · All erosion and sediment control BMPs shall be designed, constructed and maintained in all development sites in accordance with the "GTA CA's Erosion & Sediment Control Guidelines For Urban Construction" as well as City of Toronto Sewer Use By-Law and/or other City of Toronto requirements on a site by site basis, where applicable.

1.3.3 Water Balance

- a) Retained on-site, to the maximum extent practicable to achieve the same level of annual volume of overland runoff allowable from the development site under predevelopment (i.e. presently existing site conditions before the new proposed development) conditions.
- b) If the allowable annual runoff volume from the development site under postdevelopment conditions is less than the pre-development conditions, then the more

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stringent runoff volume requirement becomes the governing target for the development site.

c) Regardless of the off-site compensatory/cash-in-lieu option, the minimum on-site runoff retention requires the proponent to capture all runoff from a small design rainfall event (typically 5 mm) and restore it on-site through infiltration, evapotranspiration and rainwater reuse.

1.4 PERFORMANCE STANDARDS – CITY OF VAUGHAN

The proposed Steeles West station is located on the boundary between the City of Toronto and the Region of York, within the City of Vaughan. City staff has indicated that quality control should be in accordance with TRCA requirements, and that quantity control should ensure post to pre-development peak flows for 2 to 100-year return period events.

Furthermore, any proposed SWM works north of Steeles Avenue between Jane and Keele Streets must proceed in accordance with the stormwater management initiative that will be developed as part of the City of Vaughan's planned development in this area (OPA 620).

1.5 PERFORMANCE STANDARDS - TORONTO TRANSIT COMMISSION (TTC)

This report also considered design criteria recommendations contained in TTC's "Design Standards, Volume 1." Section 2 provides storm drainage design recommendations. The following is a summary:

- The Modified Rational Method may be used to develop hydrographs for the design of detention storage systems (Section 2.2):
- For design purposes the storm frequency shall meet the requirements of the approval authorities (Section 2.4.2.1);
- Roof storage maximum controlled run-off 42 1/s per hectare of roof area, maximum ponding depth 150 mm; surface storage maximum ponding depth of 0mm for 1:2 year storm and 250 mm for 1: 100-Year storm (Section 3.2);
- Overland flow gradients for parking lots shall be a minimum of 2% and a maximum of 4% (Section 5.2.1).

1.6 PERFORMANCE STANDARDS – TORONTO AND REGION CONSERVATION AUTHORITY (TRCA)

In accordance with TRCA's requirements, lot level conveyance controls (parking and roof-top storage) are to be designed to reduce post development peak flows for 2:100 year return periods

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to pre-development flows. Furthermore, the Toronto and Region Conservation Authority (TRCA) encourages the use of innovative lot level stormwater management controls. These practices include maximizing on-site stormwater infiltration, the retention and enhancement of pervious and vegetative area (tree and shrub plantings, infiltration trenches, grassed swales), the use of biologically-based pollutant load reduction features (bio-swales, vegetated filter strips) and the reduction of sediment and nutrient loadings through the development of, for instance, pollution prevention plans, sediment control during construction, oil-grit separators etc.

Examples of innovative of level controls may be viewed on TRCA's website (http://www.trca.on.ca); refer to the Etobicoke / Mimico Creek Strategy document, Chapter 7, page 184. These measures should be considered and incorporated where possible during detailed design. TRCA's Erosion and Sediment Control (ESC) Guidelines - December 2003, will be used as the basis for developing an Erosion and Sedimentation Control Design Brief during detailed design.

1.7 ANALYSIS METHODOLOGY

Quantity Control

For each proposed facility, the Rational Method was used to determine the pre-construction uncontrolled peak flow rate (see Appendix B). The following equation was used:

 $Q_{x \text{ year}} = CIA/360$

Where:

| C - permeability coefficient (unitless): | 0.3 for open fields was used, 0.9 for new facilities; |
|--|---|
| I - rainfall intensity (mm/hour): | based on North York IDF curve data, |
| | Tc = 10 minutes pre, 7 minutes post construction; |
| A - catchment area (hectares): | area of facility in hectares. |

City of Toronto harmonized IDF curves (presently not available) or North York District IDF curves should be used in the detailed designs.

Storage requirements using the Modified Rational Method have been provided in Appendix C. For the Finch West Station, release rates for the Humber River Watershed, Sub-Basin 46 have been provided by TRCA (provided below) and should be confirmed during detail design. Roof control (Zurn) release rates were considered for the Sheppard and York University Stations since roof leaders will discharge directly to the ground.

| 2-year | 5-year | 25-year | 100-year |
|--------|--------|---------|----------|
| | | | |

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|------------------|------------|------------|---------------|------------------|
| Allowable | Q=7.745- | Q=11.468- | Q=17.381- | Q=22.973- |
| Release Rate: | 0.762ln(A) | 1.123ln(A) | 1.690ln(A) | 2.256ln(A) |

Where for release rates: Q - unit flow (L/s/ha) - litres per second per hectare A - area in hectares (ha)

For the Steeles West Station, the ultimate SWM plan will be developed during detail design in accordance with OPA 620 requirements, and for the purposes of the interim SWM plan proposed at that Station, storage requirements are based on post to pre peak flow rates for all return periods.

For all proposed stations addressed in this SWM plan, the rational method was used to calculate peak flows. A pre-development drainage coefficient "C" of 0.3 was used, and a postdevelopment drainage coefficient "C" value of 0.9 was used. North York IDF curve coefficients (from the City of Toronto) were used as follows:

| Coefficient | 2-year | 5-year | 25-year | 100-year |
|-------------|--------|--------|---------|----------|
| а | 652.8 | 840.7 | 1082 | 1334 |
| b | 4 | 3 | 2 | 2 |
| с | 0.786 | 0.779 | 0.771 | 0.771 |

Ouality Control

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Quality control was not considered for the proposed Sheppard West and York University stations due to the absence of pollution sources at these sites (commuter parking is only being provided at the proposed Finch West and Steeles West stations). Proposed quality control for the Finch and Steeles West stations consists of Oil / Grit Separators (OGS) in a "treatment train" approach in accordance with the above noted criteria as applicable.

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Water Balance

Preliminary geotechnical information on the subsurface physical conditions (soil and groundwater) along the proposed subway route was conducted by Golder Associates Ltd. (Golder) and documented in their draft report "Geotechnical Investigation Report - Spadina Subway Extension Environmental Assessment" (December 2005). The following excerpt (page 16) summarizes the typical founding soils for the four proposed subway station base slabs:

| Station | Estimated Elevation of Base Slab (m) | Founding Soil | Soil Type |
|--------------------|---|---|-----------|
| GO/Sheppard Avenue | 180 | Silt; Clayey silt (Interstadial) | 8; 9 |
| Keele/Finch | 175 | Clayey Silt to Silty Clay Till; Clayey Silt (Interstadial) | 11; 9 |
| York University | 175 | Sandy Silt to Sand and Silt Till | 12 |
| Steeles Avenue | 180 | Clayey Silt to Silty Clay Till | 11 |

Reference is made in this geotechnical report (page 12) to the average hydraulic conductivity of 1.4E-05 to 3.0E-05 cm/s within the cohesive and glacial till deposits. Although these preliminary soils investigations indicate soils not conducive to Water Balance measures, measures will need to be addressed for each station during detail design in accordance with the above noted criteria where feasible.

On-site SWMP's considered in the following plan include rooftop restrictors (at station buildings), exfiltration systems (proposed in a "treatment train" approach with oil / grit separators) and underground storage at the proposed parking lots at Finch and Steeles Stations (super pipe for the 2-year event). Additional SWMP's to be considered during detail design include rainwater harvesting, green roof technologies, absorbent landscaping, pervious pavement in parking lots and tree plantings and bushes. Additionally, the use of curb and gutter with catchbasins and exfiltration / infiltration systems should be considered.

The following summarizes the results of the hydraulic /hydrologic analysis and identifies the proposed stormwater management plan for each proposed station location.

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CHAPTER 2.0 SHEPPARD AVENUE WEST STATION SWM PLAN

The Sheppard West Station, situated entirely within the Downsview Park lands, will be located at the southwest corner of the Bradford GO Line and Sheppard Avenue. New above ground facilities that will reduce the overall permeability within the study area include the new subway station building itself. Impervious areas associated with these new facilities are provided in Table 2.0. Refer to Exhibit 2.1 for a map of this station location including the existing drainage condition as identified from OBM maps and a site visit.

Table 2.0 - Above Ground Facilities at the Sheppard Avenue West Station

| Facility | Impervious Area Proposed (ha) |
|----------------------|-------------------------------|
| New TTC Station Roof | 0.2 |

The surface at the existing site drains generally to the north. Utility information provided by the City indicates that storm water is conveyed easterly along Sheppard Avenue through a series of storm sewers (900, 1050 mm diameter in the vicinity of the proposed station) eventually draining to the G. Ross Lord Dam and Reservoir to the north/north-east.

2.1 DESIGN REOUIREMENTS

Design of SWM facilities will be based on the criteria provided by the City of Toronto, the TTC, and TRCA as summarized in Sections 1.3 to 1.6 of this Report.

2.2 OUALITY CONTROL

Quality control was not considered for the proposed Sheppard West station due to the absence of pollution sources this site.

2.3 QUANTITY CONTROL

As indicated in Section 1.7, the Rational Method was used to determine the pre-construction uncontrolled 2 to 100-year peak flow rates. To ensure that the subject development will not have a negative impact on downstream conditions, it is necessary to control the post-development flows for each return period from 2 to 100 years to pre-development flows. For the TTC station building, rooftop storage is proposed. A separate GO Transit Environmental Assessment will be conducted for the stormwater management of the proposed new GO Transit platform.

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Exhibit 2.1 – Existing Drainage Conditions at the Proposed Sheppard West Station



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Allowable release rates were provided by TRCA (Section 1.7); however, as downspouts will outlet at ground level, and as the TTC roof storage maximum controlled run-off is 42 l/s per hectare (TTC Standard Volume 1, Section 3.2), a maximum allowable release rate was set to (42 1/s) x (0.2 ha) = 8.4 1/s.

Results are summarized in Table 2.1.

| Table 2.1 – | - Storage Requirements | s at the Sheppard Avenue | West Station |
|-------------|------------------------|--------------------------|--------------|
|-------------|------------------------|--------------------------|--------------|

| Facility | Area (ha) | Return Period | Allowable Release Rate (l/s) | Q Uncontrolled Pre-Const. (1/s) | Q Uncontrolled Post-Const. (l/s) | Volume Required (m3) |
|---------------------|--------------|------------------|------------------------------------|--|---|----------------------------|
| TTC | 0.2 | 2-year | 8.4 | 13.7 | 49.6 | 22 |
| Station Building | 0.2 | 5-year | 8.4 | 19.0 | 70.0 | 35 |
| | 0.2 | 25-year | 8.4 | 26.6 | 99.5 | 53 |
| | 0.2 | 100-year | 8.4 | 32.8 | 122.7 | 70 |

The proposed stormwater management plan for this station entails the use of quantity control through the use of Zurn Roof Control Drains in accordance with previously stated design criteria.

2.4 WATER BALANCE

As indicated in Section 1.7, the preliminary soils investigations in the vicinity of the Sheppard Ave. West station indicate soils may not be conducive to water balance measures. However, City of Toronto water balance requirements in accordance with Section 1.3.3 should be addressed during detail design.

2.5 EROSION AND SEDIMENT CONTROL

Erosion and Sediment Control will be addressed during detail design in accordance with applicable criteria in Section 1.3.2 above. During planning, it was confirmed by TRCA that criteria (c) Section 1.3.2 governs at this location.

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CHAPTER 3.0 FINCH WEST STATION SWM PLAN

The Finch West Station will be located at the intersection of Finch Avenue and Keele Street. New above ground facilities that will reduce the overall permeability of the study area include the new commuter parking lot to the east of Keele Street, the passenger pick -up and drop-off to the west of Keele Street, and the proposed bus terminal including the new roads. Impervious areas associated with these new facilities are provided in Table 3.0. Refer to Exhibit 3.1 for a map of this station location including the existing drainage condition as identified from OBM maps and a site visit.

Table 3.0 - Above ground Facilities at the Finch West Station

| Facility | Impervious Area Proposed (ha) |
|--|-------------------------------|
| Commuter Parking Lot | 2.3 |
| Passenger Pick-Up / Drop-Off | 0.3 |
| Bus Terminal / Roads / Station Building | 1.2 |

According to drainage mosaics provided by the City, the surface at the existing site generally drains to the east and west from Keele Street, with the exception of a triangular area at the northeast quadrant of the Finch / Keele intersection which also drains to the west as indicated in Exhibit 3.1. The site is drained by storm sewers, with the area west of Keele street draining towards the 5000 x 3000 mm CSP under Finch Avenue, ultimately released to the Black Creek; to the east, storm water is conveved via storm sewers and creek to the G. Lord Ross Reservoir and Dam.

3.1 DESIGN REQUIREMENTS

Design of SWM facilities will be based on criteria provided by the City of Toronto, the TTC, and TRCA as summarized in Sections 1.3 to 1.6 of this Report.

3.2 QUALITY CONTROL

To address the requirements for quality treatment on the site, oil grit separators are proposed in a treatment train approach in coordination to include for instance bio-swales and infiltration systems. Proposed flow patterns are indicated in Exhibit 3.2.

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Exhibit 3.1 - Existing Drainage Conditions at the Proposed Finch West Station



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Exhibit 3.2 – Proposed Drainage Conditions at the Proposed Finch West Station



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3.3 QUANTITY CONTROL

For the parking lot, passenger pick-up / drop-off and bus terminal, parking lot conveyance control is suggested. Results are summarized in Tables 3.1, 3.2, and 3.3.

| Facility | Area (ha) | Return Period | Allowable Release Rate (l/s) | Q Uncontrolled Pre-Const. (l/s) | Q Uncontrolled Post-Const. (1/s) | Volume Required (m3) |
|----------------|--------------|------------------|------------------------------------|---------------------------------------|---|----------------------------|
| Comm. | 2.3 | 2-year | 16.4 | 157.3 | 570.5 | 498 |
| Parking Lot | 2.3 | 5-year | 24.2 | 218.7 | 804.7 | 648 |
| | 2.3 | 25-year | 36.7 | 305.5 | 1144.3 | 840 |
| | 2.3 | 100-year | 48.5 | 376.7 | 1410.7 | 1013 |

Table 3.2 – Passenger Pick-up/Drop-off Storage Requirements at the Finch West Station

| Facility | Area (ha) | Return Period | Allowable Release Rate (l/s) | Q Uncontrolled Pre-Const. (l/s) | Q Uncontrolled Post-Const. (1/s) | Volume Required (m3) |
|------------------|--------------|------------------|------------------------------------|---------------------------------------|---|----------------------------|
| Pass. | 0.3 | 2-year | 2.6 | 20.5 | 74.4 | 61 |
| Pick-Up Drop- | 0.3 | 5-year | 3.8 | 28.5 | 105.0 | 80 |
| Off | 0.3 | 25-year | 5.8 | 39.9 | 149.3 | 103 |
| | 0.3 | 100-year | 7.7 | 49.1 | 184.0 | 124 |

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|---|--|--|--|--|--|------------------------------|------|--|--|
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| Table 3.3 – Bus Terminal Storage Requirements at the Finch West Station | | | | | | | | | |
| - | | | | | | 2 | ** 1 | | |

| Facility | Area (ha) | Return Period | Allowable Release Rate (l/s) | Q Uncontrolled Pre-Const. (l/s) | Q Uncontrolled Post-Const. (1/s) | Volume Required (m3) |
|---------------------|--------------|------------------|------------------------------------|---------------------------------------|---|----------------------------|
| Bus | 1.2 | 2-year | 9.1 | 82.1 | 297.7 | 255 |
| Roads / | 1.2 | 5-year | 13.5 | 114.1 | 419.9 | 331 |
| Station Building | 1.2 | 25-year | 20.5 | 159.4 | 597.0 | 429 |
| | 1.2 | 100-year | 27.1 | 196.5 | 736.0 | 517 |

The proposed stormwater management plan for this station entails the use of quantity control through the use of Zurn Roof Control Drains in accordance with previously stated design criteria. To further satisfy TTC site drainage requirements (see Section 1.5 above) since no ponding will be permitted under the 2-year storm event, it is proposed that the post-construction 2-year storm event be captured in a "super-pipe". Refer to Exhibit 3.2 for a map of this station location including the proposed drainage condition. It is proposed that Oil / Grit Separators (OGS) be used in a "treatment train" approach, including exfiltration trenches located in grassed boulevard areas adjacent to parking lots prior to entry into City sewer system (as the only available space is in the Hydro Corridor, this will require approval from Ontario Hydro).

3.4 WATER BALANCE

As indicated in Section 1.7, the preliminary soils investigations in the vicinity of the Finch West station indicate soils may not be conducive to water balance measures. However, City of Toronto water balance requirements in accordance with Section 1.3.3 should be addressed during detail design.

3.5 EROSION AND SEDIMENT CONTROL

Erosion and Sediment Control will be addressed during detail design in accordance with applicable criteria in Section 1.3.2 above. During planning, it was confirmed by TRCA that criteria (d) Section 1.3.2 governs at this location, however, TRCA also requested that the runoff from a 25 mm storm be detained on-site and released over a minimum of 48 hours.

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CHAPTER 4.0 YORK UNIVERSITY STATION SWM PLAN

The York University Station will be located at the east end of the "commons" within the University campus. The Subway station will be a below ground facility. New above ground facilities that will reduce the overall permeability of the study area include the substation building, as well as two entrances to the subway. Impervious areas associated with these new facilities are provided in Table 4.0. Refer to Exhibit 4.1 for a map of this station location including the existing drainage condition as identified from OBM maps and a site visit.

Table 4.0 - Above ground Facilities at the York University Station

| Facility | Impervious Area Proposed (ha) |
|-----------------------------------|-------------------------------|
| Substation Building and Entrances | 0.1 |

Surface water in the vicinity of the proposed facility drains through a series of storm sewers to the pond at Pond Road, then ultimately to the Black Creek. A ditch inlet was noted in the grassed area of the "Common", as well as on the east side of Ian MacDonald Boulevard within the existing grassed swale.

4.1 DESIGN REOUIREMENTS

Design of SWM facilities will be based on criteria provided by the City of Toronto, the TTC, and TRCA as summarized in Sections 1.3 to 1.6 of this Report.

4.2 OUALITY CONTROL

Quality control was not considered for the proposed York University station due to the absence of pollution sources (new facilities include only building roofs) at this site.

4.3 **QUANTITY CONTROL**

As indicated in Section 1.7, the Rational Method was used to determine the pre-construction uncontrolled 2 to 100-year peak flow rates. To ensure that the subject development will not have a negative impact on downstream conditions, it is necessary to control the post-development flows for each return period from 2 to 100 years to pre-development flows. For the TTC station building, rooftop storage is proposed and summarized in Table 4.1. Although peak runoff will be controlled for post to pre for the 2 to 100 year events, York University's Stormwater Management Plan should be consulted for any additional requirements prior to detailed design.

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Exhibit 4.1 – Existing Drainage Conditions at the Proposed York University Station



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Allowable release rates were provided by TRCA (Section 1.7); however, as downspouts will outlet at ground level, and as the TTC roof storage maximum controlled run-off is 42 l/s per hectare (TTC Standard Volume 1, Section 3.2), a maximum allowable release rate was set to (42 l/s) x (0.1 ha) = 4.2 l/s.

| Table 4.1 –Storage | Requirements at the | York | University | Station |
|--------------------|---------------------|------|------------|---------|
|--------------------|---------------------|------|------------|---------|

| Facility | Area (ha) | Return Period | Allowable Release Rate (l/s) | Q Uncontrolled Pre-Const. (1/s) | Q Uncontrolled Post-Const. (l/s) | Volume Required (m3) |
|---------------------|--------------|------------------|------------------------------------|--|---|----------------------------|
| TTC | 0.1 | 2-year | 4.2 | 6.8 | 24.8 | 11 |
| Station Building | 0.1 | 5-year | 4.2 | 9.5 | 35.0 | 17 |
| | 0.1 | 25-year | 4.2 | 13.3 | 49.8 | 26 |
| | 0.1 | 100-year | 4.2 | 16.4 | 61.3 | 35 |

The proposed stormwater management plan for this station entails the use of quantity control through the use of Zurn Roof Control Drains in accordance with previously stated design criteria

4.4 WATER BALANCE

As indicated in Section 1.7, the preliminary soils investigations in the vicinity of the York University station indicate soils may not be conducive to water balance measures. However, City of Toronto water balance requirements in accordance with Section 1.3.3 should be addressed during detail design.

4.5 EROSION AND SEDIMENT CONTROL

Erosion and Sediment Control will be addressed during detail design in accordance with applicable criteria in Section 1.3.2 above. During planning, it was confirmed by TRCA that criteria (c) Section 1.3.2 governs at this location.

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CHAPTER 5.0 STEELES WEST STATION SWM PLAN

The Steeles West Station will be located at the intersection of Steeles Avenue and Northwest Gate. New above ground facilities that will reduce the overall permeability of the study area include two new commuter parking lots located within the Hydro corridor north of Steeles Avenue, one bus terminal located north of Steeles Avenue including passenger pick-up and dropoff facilities and entrances. Impervious areas associated with these new facilities are provided in Table 5.0. One bus terminal is to be located south of Steeles Avenue utilizing an existing parking lot, and thereby not increasing the ground imperviousness. Refer to Exhibit 5.1 for a map of this station location including the existing drainage condition as identified from OBM maps and a site visit.

| Table 5.0 - | Above ground | Facilities at | the Steeles | West Station |
|--------------|--------------|---------------|-------------|--------------|
| 1 able 5.0 - | Above ground | racinues at | the Steeles | west station |

| Facility | Impervious Area Proposed (ha) |
|---|-------------------------------|
| New East Commuter Parking Lot | 5.2 |
| New West Commuter Parking Lot including Passenger Pick-Up and Drop-Off | 4.9 * |
| New Inter-Regional Bus Terminals (north of Steeles Avenue) / Station Buildings | 2.1 |
| New Inter-Regional Bus Terminal (south of Steeles Avenue) / Station Buildings | Area presently paved |

* Includes a portion of facilities included in York Regions Highway 7 Transitway EA.

Presently the subject land, north of Steeles and south of the Hydro corridor, is an open field where Northwest Gate intersects Steeles Avenue at an unsignalized "T" intersection. Surface drainage in the area of the proposed facility is to the south, to two sets of existing storm sewers, one under Steeles Avenue, and one just north of the right-of-way. The storm sewer under Steeles Avenue (600 to 1500 mm diameter) drains to TRCA's pond at Black Creek Pioneer Village; to the north to the right-of-way, the storm sewer (1650 to 1800 mm diameter) drains to a pond north of Steeles Avenue near Jane Street. It is assumed that the building to the east of the proposed facility manages it's own stormwater. Therefore the property boundary of the proposed parking facilities coincides with the drainage boundaries.

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Exhibit 5.1 - Existing Drainage Conditions at the Proposed Steeles West Station



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5.1 DESIGN REQUIREMENTS

Design of SWM facilities will be based on the criteria provided by the City of Toronto, the TTC, TRCA and the City of Vaughan, as summarized in Sections 1.3 to 1.6 of this Report.

According to TRCA, the existing stormwater management pond (CFN 8133, TRCA Pond File 42.0) located north of Steeles at Jane Street is inadequate by present day standards, and there is little room available to expand the pond for the redevelopment of the industrial area to the north of Steeles Avenue including the Steeles West Station. The pond is presently a peak flow attenuation facility only. Although it is not presently possible within the scope of this study to provide a definitive SWM plan for the Steeles West Station, a detailed SWM plan for the Steeles West Station will need to be integrated into a comprehensive stormwater Management master plan, once developed, in accordance with development (OPA 620) in the area.

5.2 QUALITY CONTROL

To address the **interim** requirements for quality treatment on the site (prior to a developed Master SWM Plan for the area in accordance with OPA 620), oil grit separators are proposed in a treatment train approach, to include for instance bio-swales and infiltration systems. Proposed flow patterns are indicated in **Exhibit 5.2**.

5.3 QUANTITY CONTROL

For the parking lot, passenger pick-up / drop-off and bus terminal, in-lieu of a definitive SWM Master Plan for the area, interim parking lot conveyance control is suggested. Results are summarized in **Tables 5.1, 5.2, and 5.3.** Although the east and west commuter parking lot areas approach and slightly exceed the criteria for Rational Method calculations (Section 1.3.2 above) the Rational Method was used since some portion of these facilities are actually addressed in York Region's Highway 7 Transitway EA. Furthermore, the impacts from new roads will also be addressed separately through York Region's Hwy 7 Transitway Environmental Assessment.

| Facility | Area (ha) | Return Period | Q Uncontrolled Pre-Const. (l/s) | Q Uncontrolled Post-Const. (l/s) | Volume Required (m3) | | |
|---|--------------|------------------|------------------------------------|-------------------------------------|-------------------------|--|--|
| East | 5.2 | 2-year | 355.7 | 1289.8 | 450 | | |
| Lot | 5.2 | 5-year | 494.4 | 1819.4 | 599 | | |
| | 5.2 | 25-year | 690.8 | 2587.0 | 828 | | |
| | 5.2 | 100-year | 851.7 | 3189.5 | 1020 | | |
| Table 5.2 West Commuter Dorking Let Stange Dequirements at the Stanley West Station | | | | | | | |

Table 5.2 – West Commuter Parking Lot Storage Requirements at the Steeles West Station

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|--------------|---|---|---|--|--|
| Area (ha) | Return Period | Q Uncontrolled Pre-Const. (l/s) | Q Uncontrolled Post-Const. (l/s) | Volume Required (m3) | |
| 4.9 | 2-year | 335.2 | 1215.4 | 411 | |
| 4.9 | 5-year | 465.8 | 1714.4 | 565 | |
| 4.9 | 25-year | 650.9 | 2437.8 | 780 | |
| 4.9 | 100-year | 802.5 | 3005.5 | 961 | |
| | Area (ha) 4.9 4.9 4.9 4.9 4.9 | Area (ha)Return Period4.92-year4.95-year4.925-year4.9100-year | Area (ha)Return PeriodQ Uncontrolled Pre-Const. (I/s)4.92-year335.24.95-year465.84.925-year650.94.9100-year802.5 | Area (ha)Return PeriodQ Uncontrolled Pre-Const. (1/s)Q Uncontrolled Post-Const. (1/s)4.92-year335.21215.44.95-year465.81714.44.925-year650.92437.84.9100-year802.53005.5 | |

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Table 5.3 – Bus Terminal Storage Requirements at the Steeles West Station

| Faci | lity | Area (ha) | Return Period | Q Uncontrolled Pre-Const. (l/s) | Q Uncontrolled Post-Const. (l/s) | Volume Required (m3) |
|----------|----------------------|--------------|------------------|------------------------------------|-------------------------------------|-------------------------|
| Bus | • • • | 2.1 | 2-year | 143.7 | 520.9 | 176 |
| Stati | Terminal/ Station | 2.1 | 5-year | 199.6 | 734.8 | 242 |
| Building | 2.1 | 25-year | 279.0 | 1044.8 | 334 | |
| | | 2.1 | 100-year | 343.9 | 1288.1 | 412 |

To further satisfy TTC site drainage requirements (see Section 1.5 above) since no ponding will be permitted under the 2-year storm event, it is proposed that the post-construction 2-year storm event be captured in a "super-pipe" or in swales or depressions prior to release. Refer to **Exhibit 5.2** for a map of this station location including the proposed drainage condition. It is proposed that this interim solution (ultimate SWM solution to be part of the SWM Master Plan in accordance with OPA 620), Oil / Grit Separators (OGS) be used in a "treatment train" approach, including exfiltration trenches located in grassed boulevard areas adjacent to parking lots).

5.4 WATER BALANCE

Spadina Subway Extension

As indicated in Section 1.7, the preliminary soils investigations in the vicinity of the Steeles West station indicate soils may not be conducive to water balance measures. However, City of Toronto water balance requirements according to Section 1.3.3 will be addressed in detail design.

5.5 EROSION AND SEDIMENT CONTROL

Erosion and Sediment Control will be addressed during detail design in accordance with applicable criteria in Section 1.3.2 above. During planning, it was confirmed by TRCA that criteria (d) Section 1.3.2 governs at this location, however, TRCA also requested that the runoff from a 25 mm storm be detained on-site and released over a minimum of 48 hours.

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Exhibit 5.2 – Proposed Drainage Conditions at the Proposed Steeles West Station



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CHAPTER 6.0 CONSTRUCTION IMPACTS AND MITIGATION AND MONITORING

During construction activities including dewatering, erosion and sedimentation potential will be addressed.

Governmental documentation related to erosion control and sedimentation exists in the following three forms: legislation, guidelines and by-laws. Guidelines used within TRCA's jurisdiction include current editions of the following:

- MNR Technical Guideline: Erosion and Sediment Control;
- GTA Conservation Authorities Erosion & Sediment Control Guidelines for Urban Construction;
- City of Toronto Sewer Use B-Law; and,
- MTO Drainage Management Manual.

Mitigation will be addressed in contract documents according to TRCA's Erosion and Sedimentation guidelines with explains the design, function, installation procedure, maintenance procedure, and removal procedure for each of the following ESC measures including, but not limited to sediment traps, interceptor swales/dykes, sediment control fences, straw bales, sodding etc.

Prior to construction, the contractor is required to submit comprehensive environmental controls and methods plan to address, among other elements, effluent (water control) as per TTC's Master Specification 05-06-28 – Section 01575 – subsection 6. The effectiveness of this plan is monitored during a demonstration of the process that is undertaken before the Work can commence on site. A representative of TTC will undertake monitoring of plan compliance.

The construction process will result in exposed soil in areas such as the Hydro corridors during the construction of the commuter parking lots or the Downsview lands during the open cut construction of the running structure. Sediment and erosion control measures will be inspected regularly by TTC to ensure that these measures are maintained in proper working order until all areas are fully stabilized.

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CHAPTER 7.0 CONCLUSIONS

The preliminary analysis as summarized in this report indicates that the proposed stormwater management plan for each of the 3 proposed subway stations, namely Sheppard West, Keele Street, and York University Stations will satisfy design requirements of the TTC, the City of Toronto and TRCA. The SWM plan for the Steeles West Station will require further development during detail design in accordance with a SWM Master Plan to be developed in response to development north of Steeles Avenue.

Further refinements to this plan will be required during the detailed design phase of the subway extension project.

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APPENDICES

APPENDIX A TRCA's Flood Flow Criteria Map



APPENDIX B RATIONAL METHOD CALCULATIONS

Sheppard

2-Year Pre-Development Peak Flow

| Rational M | Raint | all Intensity | | |
|----------------------|-------|---------------|-----|------------|
| Area = | 0.20 | ha | Co | efficients |
| "C" = | 0.30 | | Yo | rk Region |
| Tc = | 10.00 | min | 2 Y | ear Storm |
| AC = | 0.060 | | a = | 652.8 |
| 2.78*AC = | 0.167 | | b = | 4.00 |
| Rainfall Intensity = | 82.02 | mm/hr | C = | 0.786 |
| | | | • | |
| Runoff = | 13.7 | l/s | | |

Predevelopment

5-Year Pre-Development Peak Flow

| Rational M | Rainfall Intensity | | | | |
|----------------------|--------------------|-------|---|-------------|-------------|
| Area = | 0.20 | ha | 1 | Co | oefficients |
| "C" = | 0.30 | | | York Region | |
| Tc = | 10.00 | min | | 5 Y | ear Storm |
| AC = | 0.060 | | | a = | 840.7 |
| 2.78*AC = | 0.167 | | | b = | 3.00 |
| Rainfall Intensity = | 113.99 | mm/hr | | C = | 0.779 |
| Runoff = | 19.0 | l/s | | | |

25-Year Pre-Development Peak Flow

| Rational M | | Rain | fall Intensity | | |
|----------------------|--------|-------|----------------|--------------|------------|
| Area = | 0.20 | ha | | Coefficients | |
| "C" = | 0.30 | | | York Region | |
| Tc = | 10.00 | min | | 25 \ | Year Storm |
| AC = | 0.060 | | | a = | 1082 |
| 2.78*AC = | 0.167 | | | b = | 2.00 |
| Rainfall Intensity = | 159.29 | mm/hr | | C = | 0.771 |
| Runoff = | 26.6 | l/s | - | | |

100-Year Pre-Development Peak Flow

| Rational Method | | | Rain | fall Intensity |
|----------------------|--------|-------|------|----------------|
| Area = | 0.20 | ha | Co | oefficients |
| "C" = | 0.30 | | Yo | rk Region |
| Tc = | 10.00 | min | 100 | Year Storm |
| AC = | 0.060 | | a = | 1334 |
| 2.78*AC = | 0.167 | | b = | 2.00 |
| Rainfall Intensity = | 196.38 | mm/hr | C = | 0.771 |
| | | | | |
| Runoff = | 32.8 | l/s | | |

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| Finch Parking | Predevelopment |
|----------------------|----------------|
| 2-Year Pre-Developme | nt Peak Flow |

| Rational M | Rational Method | | | Rainf | all Intensity |
|----------------------|-----------------|-------|---|-------|---------------|
| Area = | 2.30 | ha | | Co | efficients |
| "C" = | 0.30 | | | Yo | rk Region |
| Tc = | 10.00 | min | | 2 Y | ear Storm |
| AC = | 0.690 | | 1 | a = | 652.8 |
| 2.78*AC = | 1.918 | | | b = | 4.00 |
| Rainfall Intensity = | 82.02 | mm/hr | | C = | 0.786 |
| | | | • | | |
| Runoff = | 157.3 | l/s | | | |

5-Year Pre-Development Peak Flow

| | Rational Method | | | | |
|---|---------------------|--------|-------|--|--|
| | Area = | 2.30 | ha | | |
| | "C" = | 0.30 | | | |
| | Tc = | 10.00 | min | | |
| | AC = | 0.690 | | | |
| | 2.78*AC = | 1.918 | | | |
| R | ainfall Intensity = | 113.99 | mm/hr | | |

Runoff = 218.7 I/s

25-Year Pre-Development Peak Flow

| Rational M | | Rainf | 2 | | |
|----------------------|--------|-------|---|------|---|
| Area = | 2.30 | ha | 1 | Co | e |
| "C" = | 0.30 | | | Yor | Ī |
| Tc = | 10.00 | min | | 25 Y | (|
| AC = | 0.690 | | | a = | |
| 2.78*AC = | 1.918 | | | b = | |
| Rainfall Intensity = | 159.29 | mm/hr | | C = | |
| | | | - | | |

Runoff = 305.5 l/s

100-Year Pre-Development Peak Flow Rational Method

| Rational | | Rain | d | | |
|----------------------|--------|-------|---|-----|----|
| Area = | 2.30 | ha | | Co | e |
| "C" = | 0.30 | | | Yo | rk |
| Tc = | 10.00 | min | | 100 | Y |
| AC = | 0.690 | | | a = | |
| 2.78*AC = | 1.918 | | | b = | |
| Rainfall Intensity = | 196.38 | mm/hr | | C = | |
| | | | - | | |

Runoff = 376.7 I/s



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| Raint | fall Intensity |
|-------|----------------|
| Co | efficients |
| Yo | rk Region |
| 5 Y | ear Storm |
| a = | 840.7 |
| b = | 3.00 |
| C = | 0.779 |
| | |
| | |

| all Intensity |
|---------------|
| efficients |
| k Region |
| 'ear Storm |
| 1082 |
| 2.00 |
| 0.771 |
| |
| |
| |

| Raint Co | Rainfall Intensity Coefficients | | | |
|-------------|------------------------------------|--|--|--|
| Yo | rk Region | | | |
| 100 | Year Storm | | | |
| a = | 1334 | | | |
| b = | 2.00 | | | |
| C = | 0.771 | | | |
| | | | | |
| | | | | |
| | | | | |

Finch PPUDO

Predevelopment



5-Year Pre-Development Peak Flow

| Rational M | Rational Method | | | Rainfall Intensity | | |
|----------------------|-----------------|-------|---|--------------------|-------------|--|
| Area = | 0.30 | ha | | Co | oefficients | |
| "C" = | 0.30 | | | Yo | rk Region | |
| Tc = | 10.00 | min | | 5 Y | ear Storm | |
| AC = | 0.090 | | 1 | a = | 840.7 | |
| 2.78*AC = | 0.250 | | | b = | 3.00 | |
| Rainfall Intensity = | 113.99 | mm/hr | | C = | 0.779 | |
| Runoff = | 28.5 | l/s | - | | | |

25-Year Pre-Development Peak Flow

| Rational Method | | | | Rainf | all Intensity |
|----------------------|--------|-------|---|-------|---------------|
| Area = | 0.30 | ha | | Co | efficients |
| "C" = | 0.30 | | | Yor | k Region |
| Tc = | 10.00 | min | | 25 Y | 'ear Storm |
| AC = | 0.090 | | | a = | 1082 |
| 2.78*AC = | 0.250 | | | b = | 2.00 |
| Rainfall Intensity = | 159.29 | mm/hr | | C = | 0.771 |
| Runoff = | 39.9 | l/s | - | - | |

100-Year Pre-Development Peak Flow

| Rational N | lethod | | | Rain | fall Intensity |
|----------------------|--------|-------|---|------|----------------|
| Area = | 0.30 | ha | 1 | Cc | oefficients |
| "C" = | 0.30 | | | Yo | rk Region |
| Tc = | 10.00 | min | | 100 | Year Storm |
| AC = | 0.090 | | | a = | 1334 |
| 2.78*AC = | 0.250 | | | b = | 2.00 |
| Rainfall Intensity = | 196.38 | mm/hr | | C = | 0.771 |
| | | | - | | |
| Runoff = | 49.1 | l/s | | | |

URS Canada Inc Spadina Subway Ext. SWM

Finch Bus Terminal Predevelopment

2-Year Pre-Development Peak Flow

| Rational M | lethod | | Rainf | fall Intensity |
|----------------------|--------|-------|-------|----------------|
| Area = | 1.20 | ha | Co | efficients |
| "C" = | 0.30 | | Yo | rk Region |
| Tc = | 10.00 | min | 2 Y | ear Storm |
| AC = | 0.360 | | a = | 652.8 |
| 2.78*AC = | 1.001 | | b = | 4.00 |
| Rainfall Intensity = | 82.02 | mm/hr | C = | 0.786 |
| | | | | |
| Runoff = | 82.1 | l/s | | |

5-Year Pre-Development Peak Flow

| - Y ea | ir Pre-Development Pe | ak Flow | | | | |
|--------|-----------------------|---------|-------|---|-----|----|
| | Rational M | | Rainf | а | | |
| | Area = | 1.20 | ha | | Co | e |
| | "C" = | 0.30 | | | Yo | rk |
| | Tc = | 10.00 | min | | 5 Y | e |
| | AC = | 0.360 | | | a = | |
| | 2.78*AC = | 1.001 | | | b = | |
| | Rainfall Intensity = | 113.99 | mm/hr | | C = | |
| | | | | • | | |

Runoff = 114.1 I/s

25-Year Pre-Development Peak Flow

| 23-Teal TTe-Development | cakilow | | | | |
|-------------------------|-----------------|-------|-----|-------|----------------|
| Rational M | Rational Method | | | Raint | fall Intensity |
| Area = | 1.20 | ha | | Co | oefficients |
| "C" = | 0.30 | | | Yo | rk Region |
| Tc = | 10.00 | min | | 25 \ | ear Storm |
| AC = | 0.360 | | | a = | 1082 |
| 2.78*AC = | 1.001 | | | b = | 2.00 |
| Rainfall Intensity = | 159.29 | mm/hr | | C = | 0.771 |
| Runoff = | 159.4 | l/s | - , | | |

100-Year Pre-Development Peak Flow

| Rational M | Rainf | З | | |
|----------------------|--------|-------|-------|---|
| Area = | 1.20 | ha | Co | e |
| "C" = | 0.30 | | Yor | ĺ |
| Tc = | 10.00 | min | 100 \ | ŕ |
| AC = | 0.360 | | a = | |
| 2.78*AC = | 1.001 | | b = | |
| Rainfall Intensity = | 196.38 | mm/hr | C = | |
| | | | | |

Runoff = 196.5 I/s

| 3 | of | 8 |
|---|----|---|
|---|----|---|

| all Intensity | | | | | |
|---------------|--|--|--|--|--|
| efficients | | | | | |
| rk Region | | | | | |
| ear Storm | | | | | |
| 840.7 | | | | | |
| 3.00 | | | | | |
| 0.779 | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

| all Intensity efficients | | | | | |
|-----------------------------|--|--|--|--|--|
| k Region Year Storm | | | | | |
| 1334 | | | | | |
| 2.00 | | | | | |
| 0.771 | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

York University

Predevelopment

| 2-Yea | ar Pre-Development Pe | ak Flow | | | | |
|-------|-----------------------|---------|-------|---|-------|---------------|
| | Rational Method | | | | Rainf | all Intensity |
| | Area = | 0.10 | ha | | Co | efficients |
| | "C" = | 0.30 | | | Yo | rk Region |
| | Tc = | 10.00 | min | | 2 Y | ear Storm |
| | AC = | 0.030 | | | a = | 652.8 |
| | 2.78*AC = | 0.083 | | | b = | 4.00 |
| | Rainfall Intensity = | 82.02 | mm/hr | | C = | 0.786 |
| | | | | - | | |
| | Runoff = | 6.8 | l/s | | | |

5-Year Pre-Development Peak Flow

| Rational M | lethod | | | Raint | all Intensity |
|----------------------|--------|-------|---|-------|---------------|
| Area = | 0.10 | ha | | Co | efficients |
| "C" = | 0.30 | | | Yo | rk Region |
| Tc = | 10.00 | min | | 5 Y | ear Storm |
| AC = | 0.030 | | | a = | 840.7 |
| 2.78*AC = | 0.083 | | | b = | 3.00 |
| Rainfall Intensity = | 113.99 | mm/hr | | C = | 0.779 |
| Runoff = | 9.5 | l/s | - | | |

25-Year Pre-Development Peak Flow

| Rational Method | | | | Rainfall Intensity | |
|----------------------|--------|-------|-----|--------------------|-------------|
| Area = | 0.10 | ha | 1 | Co | oefficients |
| "C" = | 0.30 | | | Yo | rk Region |
| Tc = | 10.00 | min | | 25 \ | ear Storm |
| AC = | 0.030 | | 1 | a = | 1082 |
| 2.78*AC = | 0.083 | | | b = | 2.00 |
| Rainfall Intensity = | 159.29 | mm/hr | | C = | 0.771 |
| Runoff = | 13.3 | l/s | _ ' | | |

100-Year Pre-Development Peak Flow

| Rational M | /lethod | | Rain | fall Intensity |
|----------------------|---------|-------|------|----------------|
| Area = | 0.10 | ha | Co | oefficients |
| "C" = | 0.30 | | Yo | rk Region |
| Tc = | 10.00 | min | 100 | Year Storm |
| AC = | 0.030 | | a = | 1334 |
| 2.78*AC = | 0.083 | | b = | 2.00 |
| Rainfall Intensity = | 196.38 | mm/hr | C = | 0.771 |
| | | | | |
| Runoff = | 16.4 | l/s | | |

URS Canada Inc Spadina Subway Ext. SWM

Steeles East Parking Predevelopment

2-Year Pre-Development Peak Flow

| Rational N | lethod | | | Raint | fall Intensity |
|----------------------|--------|-------|-----|-------|----------------|
| Area = | 5.20 | ha |] | Co | oefficients |
| "C" = | 0.30 | | | Yo | rk Region |
| Tc = | 10.00 | min | | 2 Y | ear Storm |
| AC = | 1.560 | |] | a = | 652.8 |
| 2.78*AC = | 4.337 | 1 | | b = | 4.00 |
| Rainfall Intensity = | 82.02 | mm/hr | | C = | 0.786 |
| Runoff = | 355.7 | l/s | • • | | |

5-Year Pre-Development Peak Flow

| Rational Method | | | | Rainfa |
|----------------------|--|---|--|--|
| Area = | 5.20 | ha | | Co |
| "C" = | 0.30 | | | Yor |
| Tc = | 10.00 | min | | 5 Ye |
| AC = | 1.560 | | | a = |
| 2.78*AC = | 4.337 | | | b = |
| Rainfall Intensity = | 113.99 | mm/hr | | C = |
| | | | | |
| Runoff = | 494.4 | l/s | | |
| | Rational M Area = "C" = Tc = AC = 2.78*AC = Rainfall Intensity = Runoff = | Rational Method Area = 5.20 "C" = 0.30 Tc = 10.00 AC = 1.560 2.78*AC = 4.337 Rainfall Intensity = 113.99 Runoff = 494.4 | Rational Method Area = 5.20 ha "C" = 0.30 min Tc = 10.00 min AC = 1.560 2.78*AC = 4.337 Rainfall Intensity = 113.99 mm/hr Runoff = 494.4 I/s | Rational Method Area = 5.20 ha "C" = 0.30 min Tc = 10.00 min AC = 1.560 2.78*AC = 4.337 Rainfall Intensity = 113.99 mm/hr Runoff = 494.4 I/s |

25-Year Pre-Development Peak Flow

| Rational Method | | | Raint | fall Intensity |
|----------------------|--------|-------|---------------|----------------|
| Area = | 5.20 | ha | Coefficients | |
| "C" = | 0.30 | | York Region | |
| Tc = | 10.00 | min | 25 Year Storm | |
| AC = | 1.560 | | a = | 1082 |
| 2.78*AC = | 4.337 | | b = | 2.00 |
| Rainfall Intensity = | 159.29 | mm/hr | C = | 0.771 |
| | | | | |
| Runoff = | 690.8 | l/s | | |

100-Year Pre-Development Peak Flow

| Rational Method | | | | Rainf | 6 | |
|----------------------|--------|-------|---|-------|---|--|
| Area = | 5.20 | ha | 1 | Co | e | |
| "C" = | 0.30 | | | Yor | ſ | |
| Tc = | 10.00 | min | | 100 ` | Y | |
| AC = | 1.560 | | | a = | | |
| 2.78*AC = | 4.337 | | | b = | | |
| Rainfall Intensity = | 196.38 | mm/hr | | C = | | |
| | | | | | - | |

Runoff = 851.7 l/s

| all Intensity | | | | | |
|---------------|--|--|--|--|--|
| efficients | | | | | |
| rk Region | | | | | |
| ear Storm | | | | | |
| 840.7 | | | | | |
| 3.00 | | | | | |
| 0.779 | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

| all Intensity | | | | |
|---------------|--|--|--|--|
| efficients | | | | |
| k Region | | | | |
| Year Storm | | | | |
| 1334 | | | | |
| 2.00 | | | | |
| 0.771 | | | | |
| | | | | |
| | | | | |
| | | | | |

Steeles West Parking Predevelopment

2-Year Pre-Development Peak Flow

| Rational Method | | | | Rain | fall Intensity |
|----------------------|-------|-------|---|--------------|----------------|
| Area = | 4.90 | ha | 1 | Coefficients | |
| "C" = | 0.30 | | | York Region | |
| Tc = | 10.00 | min | | 2 Year Storm | |
| AC = | 1.470 | | 1 | a = | 652.8 |
| 2.78*AC = | 4.087 | | | b = | 4.00 |
| Rainfall Intensity = | 82.02 | mm/hr | | C = | 0.786 |
| | | | - | | |
| Runoff = | 335.2 | l/s | | | |

5-Year Pre-Development Peak Flow

| Rational Method | | | Rain | fall Intensity |
|----------------------|--------|-------|--------------|----------------|
| Area = | 4.90 | ha | Coefficients | |
| "C" = | 0.30 | | York Region | |
| Tc = | 10.00 | min | 5 Year Storm | |
| AC = | 1.470 | | a = | 840.7 |
| 2.78*AC = | 4.087 | | b = | 3.00 |
| Rainfall Intensity = | 113.99 | mm/hr | C = | 0.779 |
| | | | | |

Runoff = 465.8 I/s

25-Year Pre-Development Peak Flow

| Rational Method | | | | Rainfall Intensity | | |
|----------------------|--------|-------|---|--------------------|------------|--|
| Area = | 4.90 | ha | | Coefficients | | |
| "C" = | 0.30 | | | York Region | | |
| Tc = | 10.00 | min | | 25 Y | 'ear Storm | |
| AC = | 1.470 | | | a = | 1082 | |
| 2.78*AC = | 4.087 | | | b = | 2.00 | |
| Rainfall Intensity = | 159.29 | mm/hr | | C = | 0.771 | |
| Runoff = | 650.9 | l/s | _ | - | | |

100-Year Pre-Development Peak Flow

| Rational Method | | | | Rainfall Intensity | | |
|----------------------|--------|-------|---|--------------------|------------|--|
| Area = | 4.90 | ha | | Coefficients | | |
| "C" = | 0.30 | | | York Region | | |
| Tc = | 10.00 | min | | 100 ` | Year Storm | |
| AC = | 1.470 | | | a = | 1334 | |
| 2.78*AC = | 4.087 | | | b = | 2.00 | |
| Rainfall Intensity = | 196.38 | mm/hr | | C = | 0.771 | |
| Runoff = | 802.5 | l/s | - | | | |

URS Canada Inc Spadina Subway Ext. SWM

Steeles Bus Terminal Predevelopment

2-Year Pre-Development Peak Flow

| Rational M | ſ | | |
|----------------------|-------|-------|---|
| Area = | 2.10 | ha | |
| "C" = | 0.30 | | ſ |
| Tc = | 10.00 | min | |
| AC = | 0.630 | | ſ |
| 2.78*AC = | 1.751 | | |
| Rainfall Intensity = | 82.02 | mm/hr | |
| | | | |
| Runoff = | 143.7 | l/s | |

Rainfa Coe York 2 Ye a = b = c =

5-Year Pre-Development Peak Flow

| Delit |
|--------|
| Rainfa |
| Coe |
| Yor |
| 5 Ye |
| a = |
| b = |
| C = |
| |
| |
| |

| 25-Year Pre-Development Peak Flow | | | | | | | |
|-----------------------------------|----------------------|--------|-------|---|--------|--|--|
| | Rational Method | | | | Rainfa | | |
| | Area = | 2.10 | ha | | Coe | | |
| | "C" = | 0.30 | | | Yor | | |
| | Tc = | 10.00 | min | | 25 Y | | |
| | AC = | 0.630 | | 1 | a = | | |
| | 2.78*AC = | 1.751 | | | b = | | |
| | Rainfall Intensity = | 159.29 | mm/hr | | C = | | |
| | | | | - | | | |
| | D.u. off | 070 0 | 1/- | | | | |

Runoff = 279.0 l/s

100-Year Pre-Development Peak Flow

| Rational M | lethod | | | Rainf | 6 | | |
|----------------------|--------|-------|---|-------|---|--|--|
| Area = | 2.10 | ha | | Co | e | | |
| "C" = | 0.30 | | | Yo | ſ | | |
| Tc = | 10.00 | min | | 100` | Y | | |
| AC = | 0.630 | | | a = | | | |
| 2.78*AC = | 1.751 | | | b = | | | |
| Rainfall Intensity = | 196.38 | mm/hr | | C = | | | |
| | | | - | | - | | |

Runoff = 343.9 l/s

7 of 8

| all Intensity |
|---------------|
| efficients |
| rk Region |
| ear Storm |
| 652.8 |
| 4.00 |
| 0.786 |
| |
| |
| |

| all Intensity | | | | |
|---------------|--|--|--|--|
| efficients | | | | |
| rk Region | | | | |
| ear Storm | | | | |
| 840.7 | | | | |
| 3.00 | | | | |
| 0.779 | | | | |
| | | | | |
| | | | | |
| | | | | |

| all Intensity | | | | | |
|---------------|--|--|--|--|--|
| efficients | | | | | |
| rk Region | | | | | |
| 'ear Storm | | | | | |
| 1082 | | | | | |
| 2.00 | | | | | |
| 0.771 | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

| all Intensity | | | | |
|---------------|--|--|--|--|
| efficients | | | | |
| rk Region | | | | |
| Year Storm | | | | |
| 1334 | | | | |
| 2.00 | | | | |
| 0.771 | | | | |
| | | | | |
| | | | | |
| | | | | |

Sheppard

2-Year Pre-Development Peak Flow

| Rational Method | | | Rain | fall Intensity |
|----------------------|-------|-------|------|----------------|
| Area = | 0.20 | ha | Co | oefficients |
| "C" = | 0.90 | | Yo | rk Region |
| Tc = | 7.00 | min | 2 Y | ear Storm |
| AC = | 0.180 | | a = | 652.8 |
| 2.78*AC = | 0.500 | | b = | 4.00 |
| Rainfall Intensity = | 99.14 | mm/hr | C = | 0.786 |
| - <i>"</i> | | ., | | |
| Runoff = | 49.6 | I/S | | |

Post Development

5-Year Pre-Development Peak Flow

| Rational Method | | | Raint | fall Intensity |
|----------------------|--------|-------|-------|----------------|
| Area = | 0.20 | ha | Co | oefficients |
| "C" = | 0.90 | | Yo | rk Region |
| Tc = | 7.00 | min | 5 Y | ear Storm |
| AC = | 0.180 | | a = | 840.7 |
| 2.78*AC = | 0.500 | | b = | 3.00 |
| Rainfall Intensity = | 139.84 | mm/hr | C = | 0.779 |
| Runoff = | 70.0 | l/s | | |

25-Year Pre-Development Peak Flow

| Rational Method | | | | Rain | fall Intensity |
|----------------------|--------|-------|---|-------|----------------|
| Area = | 0.20 | ha | | Co | oefficients |
| "C" = | 0.90 | | | Yo | rk Region |
| Tc = | 7.00 | min | | ב25 א | ear Storm |
| AC = | 0.180 | | | a = | 1082 |
| 2.78*AC = | 0.500 | | | b = | 2.00 |
| Rainfall Intensity = | 198.84 | mm/hr | | C = | 0.771 |
| Runoff = | 99.5 | l/s | - | | |

100-Year Pre-Development Peak Flow

| Rational Method | | | Rain | fall Intensity |
|----------------------|--------|-------|------|----------------|
| Area = | 0.20 | ha | Co | oefficients |
| "C" = | 0.90 | | Yo | rk Region |
| Tc = | 7.00 | min | 100 | Year Storm |
| AC = | 0.180 | | a = | 1334 |
| 2.78*AC = | 0.500 | | b = | 2.00 |
| Rainfall Intensity = | 245.15 | mm/hr | C = | 0.771 |
| | | | | |
| Runoff = | 122.7 | l/s | | |

URS Canada Inc Spadina Subway Ext. SWM

| | Finch Parking | Post Dev | elopment | |
|-------|-----------------------|----------|----------|--------|
| 2-Yea | ar Pre-Development Pe | ak Flow | | |
| | Rational M | lethod | | Rainfa |
| | Area = | 2.30 | ha | Co |
| | "C" = | 0.90 | | Yor |
| | Tc = | 7.00 | min | 2 Ye |
| | AC = | 2.070 | | a = |
| | 2.78*AC = | 5.755 | | b = |
| | Rainfall Intensity = | 99.14 | mm/hr | C = |
| | | | | |

Runoff = 570.5 l/s

5-Year Pre-Development Peak Flow

| rea | rear Pre-Development Peak Flow | | | | | | | |
|-----|--------------------------------|--------|-------|----|-----|----|--|--|
| | Rational M | | Rainf | ia | | | | |
| | Area = | 2.30 | ha | | Co | e | | |
| | "C" = | 0.90 | | | Yo | rŀ | | |
| | Tc = | 7.00 | min | | 5 Y | е | | |
| | AC = | 2.070 | | | a = | | | |
| | 2.78*AC = | 5.755 | | | b = | | | |
| | Rainfall Intensity = | 139.84 | mm/hr | | C = | | | |
| | | | | • | | _ | | |

Runoff = 804.7 l/s

25-Year Pre-Development Peak Flow

| Rational Method | | | | Rainf | 6 |
|----------------------|--------|-------|---|-------|----|
| Area = | 2.30 | ha | 1 | Co | e |
| "C" = | 0.90 | | | Yor | rl |
| Tc = | 7.00 | min | | 25 Y | '(|
| AC = | 2.070 | | | a = | |
| 2.78*AC = | 5.755 | | | b = | |
| Rainfall Intensity = | 198.84 | mm/hr | | C = | |
| | | | | | - |

Runoff = 1144.3 I/s

| 100-Year Pre-Development Peak Flow | | | | | | | |
|------------------------------------|----------------------|--------|-------|--|--|--|--|
| | Rational Method | | | | | | |
| | Area = | 2.30 | ha | | | | |
| | "C" = | 0.90 | | | | | |
| | Tc = | 7.00 | min | | | | |
| | AC = | 2.070 | | | | | |
| | 2.78*AC = | 5.755 | | | | | |
| | Rainfall Intensity = | 245.15 | mm/hr | | | | |



Runoff = 1410.7 l/s

| all Intensity | | | | | |
|---------------|--|--|--|--|--|
| efficients | | | | | |
| rk Region | | | | | |
| ear Storm | | | | | |
| 652.8 | | | | | |
| 4.00 | | | | | |
| 0.786 | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

| all Intensity | | | | | |
|---------------|--|--|--|--|--|
| efficients | | | | | |
| k Region | | | | | |
| ear Storm | | | | | |
| 840.7 | | | | | |
| 3.00 | | | | | |
| 0.779 | | | | | |
| | | | | | |
| | | | | | |

| all Intensity |
|---------------|
| efficients |
| k Region |
| 'ear Storm |
| 1082 |
| 2.00 |
| 0.771 |
| |
| |
| |

Finch PPUDO

Post Development



5-Year Pre-Development Peak Flow

| Rational M | lethod | | | Rain | fall Intensity |
|----------------------|--------|-------|---|------|----------------|
| Area = | 0.30 | ha | | Co | oefficients |
| "C" = | 0.90 | | | Yo | rk Region |
| Tc = | 7.00 | min | | 5 Y | ear Storm |
| AC = | 0.270 | | | a = | 840.7 |
| 2.78*AC = | 0.751 | | | b = | 3.00 |
| Rainfall Intensity = | 139.84 | mm/hr | | C = | 0.779 |
| Runoff = | 105.0 | l/s | _ | | |

25-Year Pre-Development Peak Flow

| Rational Method | | | | Rainfall Intensity | | |
|----------------------|--------|-------|---|--------------------|------------|--|
| Area = | 0.30 | ha | | Co | efficients | |
| "C" = | 0.90 | | | Yor | k Region | |
| Tc = | 7.00 | min | | 25 Y | 'ear Storm | |
| AC = | 0.270 | | | a = | 1082 | |
| 2.78*AC = | 0.751 | | | b = | 2.00 | |
| Rainfall Intensity = | 198.84 | mm/hr | | C = | 0.771 | |
| Runoff = | 149.3 | l/s | - | - | | |

100-Year Pre-Development Peak Flow

| Rational M | Rational Method | | | Rainfall Intensity | | |
|----------------------|-----------------|-------|--|--------------------|------------|--|
| Area = | 0.30 | ha | | Coefficients | | |
| "C" = | 0.90 | | | York Region | | |
| Tc = | 7.00 | min | | 100 | Year Storm | |
| AC = | 0.270 | | | a = | 1334 | |
| 2.78*AC = | 0.751 | | | b = | 2.00 | |
| Rainfall Intensity = | 245.15 | mm/hr | | C = | 0.771 | |
| | | | | | | |
| Runoff = | 184.0 | l/s | | | | |

URS Canada Inc Spadina Subway Ext. SWM

Finch Bus Terminal Post Development

2-Year Pre-Development Peak Flow

| Rational Method | | | Rainfall Intensity | | |
|----------------------|-------|-------|--------------------|------------|--|
| Area = | 1.20 | ha | Co | efficients | |
| "C" = | 0.90 | | York Region | | |
| Tc = | 7.00 | min | 2 Y | ear Storm | |
| AC = | 1.080 | | a = | 652.8 | |
| 2.78*AC = | 3.002 | | b = | 4.00 | |
| Rainfall Intensity = | 99.14 | mm/hr | C = | 0.786 | |
| | | | | | |
| Runoff = | 297.7 | l/s | | | |

5-Year Pre-Development Peak Flow

| Rational Method | | | | | |
|----------------------|--------|-------|--|--|--|
| Area = | 1.20 | ha | | | |
| "C" = | 0.90 | | | | |
| Tc = | 7.00 | min | | | |
| AC = | 1.080 | | | | |
| 2.78*AC = | 3.002 | | | | |
| Rainfall Intensity = | 139.84 | mm/hr | | | |
| - | | | | | |

Runoff = 419.9 I/s

25-Year Pre-Development Peak Flow

| | Rational Method | | | | Rainf | all Intensity | | |
|--|----------------------|--------|-------|--|-------|---------------|--|--|
| | Area = | 1.20 | ha | | Co | efficients | | |
| | "C" = | 0.90 | | | Yor | k Region | | |
| | Tc = | 7.00 | min | | 25 Y | ear Storm | | |
| | AC = | 1.080 | | | a = | 1082 | | |
| | 2.78*AC = | 3.002 | | | b = | 2.00 | | |
| | Rainfall Intensity = | 198.84 | mm/hr | | C = | 0.771 | | |
| | Runoff = | 597.0 | l/s | | | | | |

100-Year Pre-Development Peak Flow

| Rational M | | Rainfa | | | | | |
|----------------------|--------|--------|---|-------|--|--|--|
| Area = | 1.20 | ha | 1 | Co | | | |
| "C" = | 0.90 | | | Yor | | | |
| Tc = | 7.00 | min | | 100 ነ | | | |
| AC = | 1.080 | | | a = | | | |
| 2.78*AC = | 3.002 | | | b = | | | |
| Rainfall Intensity = | 245.15 | mm/hr | | C = | | | |
| | | | - | | | | |

Runoff = 736.0 l/s

| Raint | fall Intensity |
|-------|----------------|
| Co | efficients |
| Yo | rk Region |
| 5 Y | ear Storm |
| a = | 840.7 |
| b = | 3.00 |
| C = | 0.779 |
| | |
| | |
| | |

| all Intensity efficients |
|-----------------------------|
| k Region Year Storm |
| 1334 |
| 2.00 |
| 0.771 |
| |
| |
| |

York University

Post Development

| 2-Year Pre-Development Peak Flow | | | | | | |
|----------------------------------|----------------------|-------|-------|-------|---------------|-------|
| | Rational Method | | | Rainf | all Intensity | |
| | Area = | 0.10 | ha | | Coefficients | |
| | "C" = | 0.90 | | | York Region | |
| | Tc = | 7.00 | min | | 2 Year Storm | |
| | AC = | 0.090 | | | a = | 652.8 |
| | 2.78*AC = | 0.250 | | | b = | 4.00 |
| | Rainfall Intensity = | 99.14 | mm/hr | | C = | 0.786 |
| | | | | | _ | |
| | Runoff = | 24.8 | l/s | | | |

5-Year Pre-Development Peak Flow

| Rational Method | | | | Raint | all Intensity |
|----------------------|--------|-------|---|--------------|---------------|
| Area = | 0.10 | ha | 1 | Co | efficients |
| "C" = | 0.90 | | | York Region | |
| Tc = | 7.00 | min | | 5 Year Storm | |
| AC = | 0.090 | | | a = | 840.7 |
| 2.78*AC = | 0.250 | | | b = | 3.00 |
| Rainfall Intensity = | 139.84 | mm/hr | | C = | 0.779 |
| Runoff = | 35.0 | l/s | - | | |

25-Year Pre-Development Peak Flow

| Rational Method | | | | Rain | fall Intensity |
|----------------------|--------|-------|---|---------------|----------------|
| Area = | 0.10 | ha | | Coefficients | |
| "C" = | 0.90 | | | York Region | |
| Tc = | 7.00 | min | | 25 Year Storm | |
| AC = | 0.090 | | 1 | a = | 1082 |
| 2.78*AC = | 0.250 | | | b = | 2.00 |
| Rainfall Intensity = | 198.84 | mm/hr | | C = | 0.771 |
| Runoff = | 49.8 | l/s | - | | |

100-Year Pre-Development Peak Flow

| Rational Method | | | | Rain | fall Intensity |
|----------------------|--------|-------|---|------|----------------|
| Area = | 0.10 | ha | | Co | oefficients |
| "C" = | 0.90 | | | Yo | rk Region |
| Tc = | 7.00 | min | | 100 | Year Storm |
| AC = | 0.090 | | | a = | 1334 |
| 2.78*AC = | 0.250 | | | b = | 2.00 |
| Rainfall Intensity = | 245.15 | mm/hr | | C = | 0.771 |
| | | | - | | |
| Runoff = | 61.3 | l/s | | | |

URS Canada Inc Spadina Subway Ext. SWM

Steeles East Parking Post Development

2-Year Pre-Development Peak Flow

| Rational M | lethod | | Raint | fall Intensity |
|----------------------|--------|-------|--------------|----------------|
| Area = | 5.20 | ha | Co | efficients |
| "C" = | 0.90 | | York Region | |
| Tc = | 7.00 | min | 2 Year Storm | |
| AC = | 4.680 | | a = | 652.8 |
| 2.78*AC = | 13.010 | | b = | 4.00 |
| Rainfall Intensity = | 99.14 | mm/hr | C = | 0.786 |
| Runoff = | 1289.8 | l/s | | |

5-Year Pre-Development Peak Flow

| Rational Method | | | | Rainf | а |
|----------------------|--------|-------|---|-------|----|
| Area = | 5.20 | ha | | Co | e |
| "C" = | 0.90 | | | Yo | rk |
| Tc = | 7.00 | min | | 5 Y | e |
| AC = | 4.680 | | 1 | a = | |
| 2.78*AC = | 13.010 | | | b = | |
| Rainfall Intensity = | 139.84 | mm/hr | | C = | |
| | | | - | - | |
| Runoff = | 1819.4 | l/s | | | |

25-Year Pre-Development Peak Flow

| Rational Method | | | | Raint | fall Intensity |
|----------------------|--------|-------|---|---------------|----------------|
| Area = | 5.20 | ha | | Coefficients | |
| "C" = | 0.90 | | | York Region | |
| Tc = | 7.00 | min | | 25 Year Storm | |
| AC = | 4.680 | | | a = | 1082 |
| 2.78*AC = | 13.010 | | | b = | 2.00 |
| Rainfall Intensity = | 198.84 | mm/hr | | C = | 0.771 |
| | | | - | | |
| Runoff = | 2587.0 | l/s | | | |

100-Year Pre-Development Peak Flow

| ear i le Betelepinene | | | | |
|---------------------------|--------|-------|--------------|---|
| Rational Method | | | Rainf | 2 |
| Area = | 5.20 | ha | Co | e |
| "C" = | 0.90 | | Yor | ĺ |
| Tc = | 7.00 | min | 100 ` | ť |
| AC = | 4.680 | | a = | |
| 2.78*AC = | 13.010 | | b = | |
| Rainfall Intensity = | 245.15 | mm/hr | C = | |
| | | | | - |

Runoff = 3189.5 l/s

| all Intensity | | | | | |
|---------------|--|--|--|--|--|
| efficients | | | | | |
| k Region | | | | | |
| ear Storm | | | | | |
| 840.7 | | | | | |
| 3.00 | | | | | |
| 0.779 | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

| all Intensity |
|---------------|
| efficients |
| k Region |
| Year Storm |
| 1334 |
| 2.00 |
| 0.771 |
| |
| |
| |

Steeles West Parking Post Development

2-Year Pre-Development Peak Flow

| Rational M | Nethod | | | Rain | fall Intensity |
|----------------------|--------|-------|---|------|----------------|
| Area = | 4.90 | ha | 1 | Co | oefficients |
| "C" = | 0.90 | | | Yo | rk Region |
| Tc = | 7.00 | min | | 2 Y | ear Storm |
| AC = | 4.410 | | | a = | 652.8 |
| 2.78*AC = | 12.260 | | | b = | 4.00 |
| Rainfall Intensity = | 99.14 | mm/hr | | C = | 0.786 |
| | | | - | | |
| Runoff = | 1215.4 | l/s | | | |

5-Year Pre-Development Peak Flow

| Rational M | lethod | | Rain | all Intensity |
|----------------------|--------|-------|------|---------------|
| Area = | 4.90 | ha | Co | efficients |
| "C" = | 0.90 | | Yo | rk Region |
| Tc = | 7.00 | min | 5 Y | ear Storm |
| AC = | 4.410 | | a = | 840.7 |
| 2.78*AC = | 12.260 | | b = | 3.00 |
| Rainfall Intensity = | 139.84 | mm/hr | C = | 0.779 |
| | | | | |

Runoff = 1714.4 I/s

25-Year Pre-Development Peak Flow

| Rational M | /lethod | | | Rainf | all Intensity |
|----------------------|---------|-------|---|-------|---------------|
| Area = | 4.90 | ha | | Co | efficients |
| "C" = | 0.90 | | | Yo | rk Region |
| Tc = | 7.00 | min | | 25 Y | ear Storm |
| AC = | 4.410 | | | a = | 1082 |
| 2.78*AC = | 12.260 | | | b = | 2.00 |
| Rainfall Intensity = | 198.84 | mm/hr | | C = | 0.771 |
| Runoff = | 2437.8 | l/s | - | | |

100-Year Pre-Development Peak Flow

| Rational M | lethod | | Rainfall Intensity | | fall Intensity |
|----------------------|--------|-------|--------------------|-----|----------------|
| Area = | 4.90 | ha | | Co | pefficients |
| "C" = | 0.90 | | | Yo | rk Region |
| Tc = | 7.00 | min | | 100 | Year Storm |
| AC = | 4.410 | | | a = | 1334 |
| 2.78*AC = | 12.260 | | | b = | 2.00 |
| Rainfall Intensity = | 245.15 | mm/hr | | C = | 0.771 |
| Runoff = | 3005.5 | l/s | - | - | |

URS Canada Inc Spadina Subway Ext. SWM

Steeles Bus Terminal Post Development

2-Year Pre-Development Peak Flow

| Rational M | lethod | |
|----------------------|--------|-------|
| Area = | 2.10 | ha |
| "C" = | 0.90 | |
| Tc = | 7.00 | min |
| AC = | 1.890 | |
| 2.78*AC = | 5.254 | |
| Rainfall Intensity = | 99.14 | mm/hr |
| | | |
| Runoff = | 520.9 | l/s |

5-Year Pre-Development Peak Flow

| Rational N | lethod | | Ra |
|----------------------|--------|-------|----|
| Area = | 2.10 | ha | (|
| "C" = | 0.90 | | Ì |
| Tc = | 7.00 | min | 5 |
| AC = | 1.890 | | а |
| 2.78*AC = | 5.254 | | b |
| Rainfall Intensity = | 139.84 | mm/hr | С |
| | | | |
| Runoff – | 734 8 | l/e | |

ainfa Coe Yorl 5 Ye a = b = c =

Runoff = 734.8 l/s

25-Year Pre-Development Peak Flow

| 5-Y E | ear Pre-Development P | eak Flow | | | | |
|--------------|-----------------------|----------|-------|---|-------|---|
| | Rational M | lethod | | | Rainf | 2 |
| | Area = | 2.10 | ha | | Co | e |
| | "C" = | 0.90 | | | Yor | Ī |
| | Tc = | 7.00 | min | | 25 Y | 1 |
| | AC = | 1.890 | | 1 | a = | |
| | 2.78*AC = | 5.254 | | | b = | |
| | Rainfall Intensity = | 198.84 | mm/hr | | C = | |
| | | | | _ | | |
| | _ " | | | | | |

Runoff = 1044.8 l/s

100-Year Pre-Development Peak Flow

| | | | | |
|----------------------|--------|-------|-------|----|
| Rational N | lethod | | Rainf | 2 |
| Area = | 2.10 | ha | Co | e |
| "C" = | 0.90 | | Yo | rl |
| Tc = | 7.00 | min | 100` | Y |
| AC = | 1.890 | | a = | |
| 2.78*AC = | 5.254 | | b = | |
| Rainfall Intensity = | 245.15 | mm/hr | C = | |
| | | | - | - |

Runoff = 1288.1 I/s

7 of 8

| Raint | fall Intensity |
|-------|----------------|
| Co | efficients |
| Yo | rk Region |
| 2 Y | ear Storm |
| a = | 652.8 |
| b = | 4.00 |
| C = | 0.786 |
| | |
| | |
| | |

| all Intensity |
|---------------|
| efficients |
| rk Region |
| ear Storm |
| 840.7 |
| 3.00 |
| 0.779 |
| |
| |
| |

| all Intensity |
|---------------|
| efficients |
| rk Region |
| 'ear Storm |
| 1082 |
| 2.00 |
| 0.771 |
| |
| |
| |

| all Intensity | | |
|---------------|--|--|
| rk Region | | |
| Year Storm | | |
| 1334 | | |
| 2.00 | | |
| 0.771 | | |
| | | |
| | | |
| | | |

APPENDIX C MODIFIED RATIONAL METHOD STORAGE CALCULATIONS

| | | 5 | Modi | fied Ration | nal Method | | |
|-------------------|--------------|---------------|------------|---------------|------------|---------|------|
| | Pro | ject Name : | Spadian EA | | | |] |
| | 574 S | 1 | Sheppard W | est Station B | uilding | 2 | 4 |
| | F | Project No. : | 33015347 | | | | |
| | | Area = | 0.2 | ha | | | |
| | | "C" = | 0.9 | | | | |
| | | AC= | 0.18 | | | | |
| | | Tc = | 7.0 | min | | | |
| | Time | Increment = | 5.0 | min | | | - |
| | Re | lease Rate = | 8.4 | 1/s | North York | 2yr | |
| | Ma | x.Storage = | 22 | m3 | a= | 652.8 | |
| | | _ | | - | b= | 4.00 | |
| | | | | | c= | 0.786 | |
| | | | | | | | 51 |
| | Time | Rainfall | Storm | Runoff | Released | Storage | |
| | | Intensity | Runoff | Volume | Volume | Volume | |
| | (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| | 7.0 | 99.1 | 49.61 | 20.8 | 3.5 | 17.3 | |
| | 12.0 | 73.8 | 36.95 | 26.6 | 6.0 | 20.6 | |
| | 17.0 | 59.6 | 29.84 | 30.4 | 8.6 | 21.9 | |
| | 22.0 | 50.4 | 25.23 | 33,3 | 11.1 | 22.2 | <<<< |
| | 27.0 | 43.9 | 21.97 | 35.6 | 13.6 | 22.0 | |
| | 32.0 | 39.0 | 19.54 | 37.5 | 16.1 | 21.4 | |
| | 37.0 | 25.0 | 17.64 | 30.2 | 19.6 | 20.5 | |
| | 57.0 | 32.2 | 17.04 | ,19.2 | 18.0 | 20.5 | |
| | 42.0 | 32.2 | 16.11 | 40.6 | 21.2 | 19.4 | |
| | 47.0 | 29.7 | 14.86 | 41.9 | 23.7 | 18.2 | |
| | 52.0 | 27.6 | 13.80 | 43.1 | 26.2 | 16.9 | |
| | 57.0 | 25.8 | 12.91 | 44.1 | 28.7 | 15.4 | |
| | 62.0 | 24.2 | 12.13 | 45.1 | 31.2 | 13.9 | |
| | 67.0 | 22.9 | 11.46 | 46.1 | 33.8 | 12.3 | |
| | 72.0 | 21.7 | 10.86 | 46.9 | 36.3 | 10.6 | |
| | 77.0 | 20.6 | 10.33 | 47.7 | 38.8 | 8.9 | |
| | 82.0 | 19.7 | 9.85 | 48.5 | 41.3 | 1.2 | |
| | 07.U 92.0 | 10.0 | 9.43 | 49.2 | 45.8 | 2.5 | |
| 8. ₁₁₂ | 97.0 | 17.4 | 8.68 | 50.5 | 48.9 | 17 | 8 |
| 12 | 102.0 | 16.7 | 8,36 | 51.2 | 51.4 | -0.2 | |
| | 107.0 | 16.1 | 8.06 | 51.8 | 53.9 | -2.2 | |
| | 112.0 | 15.6 | 7.79 | 52.3 | 56.4 | -4.1 | |
| | 117.0 | 15.1 | 7.53 | 52.9 | 59.0 | -6.1 | |
| | 122.0 | 14.6 | 7 20 | 52 4 | 615 | 0.1 | 1 |

| | F | | Modi | fied Ratio | nal Method | | |
|---|----------|---------------|------------|---------------|------------|---------|------|
| | Pr | oject Name : | Spadian EA | | | |] |
| | | | Sheppard W | est Station I | Building | | 1 |
| | | Project No: : | 33015347 | | | | 1 |
| | | | | | | | ÷ |
| | | Area = | 0.2 | ha | | | |
| | | "C" = | 0.9 | | | | |
| | | AC= | 0.18 | | | | |
| | | Tc = | 7.0 | min | 10 | | |
| | Time | Increment = | 5.0 | min | | | |
| | Re | lease Rate = | 8.4 | l/s | North York | 5vr | 1 |
| | M | ax.Storage = | 35 | m3 | a= | 840.7 | |
| | | 0 | 1 | 1 | | 3.00 | |
| | | | | | c= | 0.779 | |
| | | | | | - | 0.1.75 | IJ |
| | Time | Rainfall | Storm | Runoff | Released | Storage |] |
| | | Intensity | Runoff | Volume | Volume | Volume | |
| | (min) | (mm/hr) | (1/s) | (m3) | (m3) | (m2) | |
| | 7.0 | 139.8 | 69.98 | 29.4 | 3.5 | 25.9 | |
| | 12.0 | 102.0 | 51.03 | 36.7 | 60 | 30.7 | |
| | 17.0 | 81.5 | 40.78 | 41.6 | 8.6 | 33.0 | |
| | 22.0 | 68.5 | 34.27 | 45.2 | 11.1 | 34.2 | |
| | 27.0 | 59.4 | 29.74 | 48.2 | 13.6 | 34.6 | |
| | 32.0 | 52.7 | 26.37 | 50.6 | 16.1 | 34.5 | |
| | 37.0 | 47.5 | 23.77 | 52.8 | 18.6 | 34.1 | |
| | 42.0 | 43.3 | 21.68 | 54.6 | 21.2 | 33.5 | |
| | 47.0 | 39.9 | 19.97 | 56.3 | 23.7 | 32.6 | |
| 3 | 52.0 | 37.1 | 18.54 | 57.9 | 26.2 | 31.7 | |
| | 57.0 | 34.6 | 17.33 | 59.3 | 28.7 | 30.5 | |
| | 62.0 | 32.5 | 16.28 | 60.6 | 31,2 | 29.3 | |
| | 67.0 | 30.7 | 15.37 | 61.8 | 33.8 | 28.0 | |
| | 72.0 | 29.1 | 14.56 | 62.9 | 36.3 | 26.6 | |
| | 77.0 | 27.7 | 13.85 | 64.0 | 38.8 | 25.2 | - 11 |
| | 82.0 | 26.4 | · 13.21 | 65.0 | 41.3 | 23.7 | |
| | 87.0 | 25.3 | 12.64 | 66.0 | 43.8 | 22.1 | |
| | 92.0 | 24.2 | 12.11 | 66.9 | 46.4 | 20.5 | |
| | 97.0 | 23.3 | 11.64 | 67.7 | 48.9 | 18.9 | |
| | 102.0 | 22.4 | 11.21 | 68.6 | 51.4 | 17.2 | |
| | 107.0 | 21.6 | 10.81 | 69.4 | 53.9 | 15.5 | |
| | 112.0 | 20.9 | 10.44 | 70.2 | 56.4 | 13.7 | |
| | 117.0 | 20.2 | 10.10 | 70.9 | 59.0 | 11.9 | |
| | 122.0 | 19.6 | 9.78 | 71.6 | 61.5 | 10.1 | |

| | | Modi | fied Ratio | nal Method | | |
|-------|---------------|------------|---------------|------------|---------|------|
| Pro | oject Name : | Spadian EA | | | | |
| | | Sheppard W | est Station I | Building | |] |
|] | Project No. : | 33015347 | | | | |
| | Area = | 0.2 | lha | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 0.18 | | | | |
| à | Tc = | 7.0 | min | | | |
| Time | Increment = | 5.0 | min | | | |
| Re | lease Rate = | 8.4 | L/s | North York | 25vr | 1 |
| Ma | ax.Storage = | 53 | m3 | a= | 1082 | |
| | U | | 1 | h= | 2.00 | |
| | | | | c= | 0.771 | 1 |
| | | | | 222 | L | 과 |
| Time | Rainfall | Storm | Runoff | Released | Storage | |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| 7.0 | 198.8 | 99.50 | 41.8 | 3.5 | 38.3 | |
| 12.0 | 141.4 | 70.77 | 51.0 | 6.0 | 44.9 | |
| 17.0 | 111.8 | 55.93 | 57.0 | 8.6 | 48.5 | |
| 22.0 | 93.3 | 46.71 | 61.7 | 11.1 | 50.6 | |
| 27.0 | 80.7 | 40.37 | 65.4 | 13.6 | 51.8 | |
| 32.0 | 71.4 | 35.71 | 68.6 | 16.1 | 52.4 | |
| 37.0 | 64.2 | 32.12 | 71.3 | 18.6 | 52,7 | <<<< |
| 42.0 | 58.5 | 29.27 | 73.8 | 21.2 | 52.6 | |
| 47.0 | 53.8 | 26.94 | 76.0 | 23.7 | 52.3 | |
| 52.0 | 50.0 | 25.00 | 78.0 | 26.2 | 51.8 | |
| 57.0 | 46.7 | 23.35 | 79.8 | 28.7 | 51.1 | |
| 62.0 | 43.8 | 21.93 | 81.6 | 31,2 | 50.3 | |
| 67.0 | 41.3 | 20.69 | 83.2 | 33.8 | 49.4 | |
| 72.0 | 39.2 | 19.61 | 84.7 | 36.3 | 48.4 | |
| 77.0 | 37.3 | 18.64 | 86.1 | 38.8 | 47.3 | |
| 82.0 | 35.5 | 17.78 | 87.5 | 41.3 | 46.1 | |
| 87.0 | 34.0 | 17.00 | 88.8 | 43.8 | 44.9 | |
| 92.0 | 32.6 | 16.30 | 90.0 | 46.4 | 43.6 | |
| 97.0 | 31.3 | 15.66 | 91.2 | 48.9 | 42.3 | |
| 102.0 | 30.1 | 15.08 | 92.3 | 51.4 | 40.9 | |
| 107.0 | 29.1 | 14.54 | 93.4 | 53.9 | 39.4 | |
| 112.0 | 28.1 | 14.05 | 94.4 | 56.4 | 38.0 | |
| | 21.2 | 15.39 | 95.4 | 59.0 | 36.5 | |

| _ | | IVIOD | med Ratio | onal Method | |
|-------|---------------|------------|--------------|-------------|---------|
| Pr | oject Name : | Spadian EA | 1 | | |
| | D ' / NT | Sheppard V | Vest Station | Building | |
| | Project No. : | 33015347 | | | 54772V |
| | Area = | 0.2 | lha | | |
| | "C" = | 0.9 | - | | |
| | AC= | 0.18 | | | |
| | Tc = | 7.0 | min | | |
| Time | Increment = | 5.0 | min | | |
| Re | elease Rate = | 8.4 | l/s | North York | 100vr |
| М | ax.Storage = | 70 | m3 | a= | 1334 |
| | - 1 | | 4J | b= | 2.00 |
| | | | | c= | 0.771 |
| | | | | · · · · | |
| Time | Rainfall | Storm | Runoff | Released | Storage |
| | Intensity | Runoff | Volume | Volume | Volume |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) |
| 7.0 | 245.2 | 122.67 | 51.5 | 3.5 | 48.0 |
| 12.0 | 174.4 | 87.26 | 62.8 | 6.0 | 56.8 |
| 17.0 | 137.8 | 68.95 | 70.3 | 8.6 | 61.8 |
| 22.0 | 115.1 | 57.59 | 76.0 | | 64.9 |
| 27.0 | 99.5 | 49 77 | 80.6 | 13.6 | 67.0 |
| 32.0 | 88.0 | 44.03 | 84.5 | 16.1 | 68.4 |
| 37.0 | 79.1 | 39.61 | 87.9 | 18.6 | 69.3 |
| 42.0 | 72.1 | 36.09 | 90.9 | 21.2 | 69.8 |
| 47.0 | 66.4 | 33.21 | 93.7 | 23.7 | 70.0 |
| 52.0 | 61.6 | 30.82 | 96.2 | 26.2 | 69.9 |
| 57.0 | 57.5 | 28.78 | 98.4 | 28.7 | 69.7 |
| 62.0 | 54.0 | 27.03 | 100.6 | 31.2 | 69.3 |
| 67.0 | 51.0 | 25.51 | 102.6 | 33.8 | 68.8 |
| 72.0 | 48.3 | 24.17 | 104.4 | 36.3 | 68.1 |
| 77.0 | 45.9 | 22.98 | 106.2 | 38.8 | 67.4 |
| 82.0 | 43.8 | 21.92 | 107.8 | 41.3 | 66.5 |
| 87.0 | 41.9 | 20.96 | 109.4 | 43.8 | 65.6 |
| 92.0 | 40.2 | 20.10 | 111.0 | 46.4 | 64.6 |
| 97.0 | 38.6 | 19.31 | 112.4 | 48.9 | 63.5 |
| 102.0 | 37,2 | 18.59 | 113.8 | 51.4 | 62.4 |
| 107.0 | 35.8 | 17.93 | 115.1 | 53.9 | 61.2 |
| 112.0 | 34.6 | 17.32 | 116.4 | 56.4 | 60.0 |
| 117.0 | 33.5 | 16.76 | 117.6 | 59.0 | 58.7 |

| | | Modi | fied Ratio | nal Method | | |
|-------|---------------|----------------|-------------|------------|----------------|---|
| Pr | oject Name : | Spadian EA | 2 | | | 1 |
| | | Finch West | Parking Lot | | |] |
| ļ | Project No. : | 33015347 | 5.4 5 | | | |
| | | | 7 | | | |
| | Area = | 2.3 | ha | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 2.07 | | | | |
| | Tc = | 7.0 | min | | | |
| Time | Increment = | 10.0 | min | (| | a |
| Re | lease Rate = | 16.4 | 1/s | North York | 2yr | |
| Ma | ax.Storage = | 498 | m3 | a= | 652.8 | |
| | | | | b= | 4.00 | |
| | | | | c= | 0.786 | |
| | | | r | | | ก |
| Time | Rainfall | Storm | Runoff | Released | Storage | |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| 7.0 | 99,1 | 570.51 | 239.6 | 6.9 | 232.7 | |
| 17.0 | 59.6 | 343.19 | 350.1 | 16.7 | 333.3 | |
| 27.0 | 43.9 | 252.69 | 409.4 | 26.6 | 382.8 | |
| 37.0 | 35.2 | 202.84 | 450.3 | 36.4 | 413.9 | |
| 47.0 | 29.7 | 170.86 | 481.8 | 46.2 | 435.6 | |
| 57.0 | 25.8 | 148.43 | 507.6 | 56.1 | 451.5 | |
| 67.0 | 22.9 | 131.74 | 529.6 | 65.9 | 463.7 | |
| 77.0 | 20.6 | 110 70 | 540 7 | 75.0 | 472.0 | |
| 77.0 | 20.0 | 110.70 | 346.7 | 73.8 | 473.0 | |
| 87.0 | 18.8 | 108.39 | 505.8 | 85.0 | 480.2 | |
| 97.0 | 17.4 | 99.86 | 581.2 | 95.4 | 485.7 | |
| 107.0 | 16.1 | 92.72 | 595.3 | 105.3 | 490.0 | |
| 117.0 | 15.1 | 86.64 | 608.2 | 115.1 | 493.1 | |
| 127.0 | 14.1 | 81.40 | 620.3 | 125.0 | 495.3 | |
| 137.0 | 13.4 | 70.83 | 631.5 | 134.8 | 496.7 | |
| 147.0 | 12.7 | 12.80 69.22 | 652.1 | 144.0 | 497.4 107.4 | |
| 167.0 | 11.0 | 66.02 | 661.5 | 164.3 | 497.0 | |
| 177.0 | 11.0 | 63.13 | 670.5 | 174.2 | 496 3 | |
| 187.0 | 10.5 | 60.52 | 679.0 | 184.0 | 495.0 | |
| 197.0 | 10.1 | 58.14 | 687.2 | 193.8 | 493.4 | |
| 207.0 | 9.7 | 55.96 | 695.1 | 203.7 | 491.4 | |
| 217.0 | 9.4 | 53.96 | 702.6 | 213.5 | 489.1 | |
| 227.0 | 9.1 | 52.12 | 709.9 | 223.4 | 486.5 | |
| 237.0 | 8.8 | 50.41 | 716.9 | 233.2 | 483.6 | |

| _ | | Modi | ned Ratic | nai Method | | |
|-------|---------------|------------|-------------|------------|---------|---|
| Pr | oject Name : | Spadian EA | L | | | 1 |
| 8 | | Finch West | Parking Lot | | | |
| | Project No. : | 33015347 | | | |] |
| | Area = | 2.3 | ha | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 2.07 | | | | |
| | Tc = | 7.0 | lmin | | | |
| Time | Increment = | 10.0 | min | | | |
| Re | lease Rate = | 36.7 | 1/s | North York | 25vr | ٦ |
| M | ax.Storage = | 840 | m3 | a= | 1082 | 1 |
| | 5 1 | 2 | Ŧ. | h= | 2.00 | |
| | | | | c= | 0.771 | ╢ |
| | | | | | | 1 |
| Time | Rainfall | Storm | Runoff | Released | Storage | 1 |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| 7.0 | 198.8 | 1144.25 | 480.6 | 15.4 | 465.2 | |
| 17.0 | 111.8 | 643.17 | 656.0 | 37.4 | 618.6 | ł |
| 27.0 | 80.7 | 464.23 | 752.1 | 59.5 | 692.6 | |
| 37.0 | 64.2 | 369.43 | 820.1 | 81.5 | 738.7 | |
| 47.0 | 53.8 | 309.81 | 873.7 | 103.5 | 770.2 | |
| 57.0 | 46.7 | 268.48 | 918.2 | 125.5 | 792.7 | |
| 67.0 | 41.3 | 237.95 | 956.6 | 147.5 | 809.0 | |
| 77.0 | 37.3 | 214.37 | 990.4 | 169.6 | 820.9 | |
| 87.0 | 34,0 | 195.55 | 1020.8 | 191.6 | 829.2 | |
| 97.0 | 31.3 | 180.14 | 1048.4 | 213.6 | 834.8 | |
| 107.0 | 29.1 | 167.26 | 1073.8 | 235.6 | 838.2 | |
| 117.0 | 27.2 | 156.31 | 1097.3 | 257.6 | 839,7 | |
| 127.0 | 25.5 | 146.89 | 1119.3 | 279.7 | 839.6 | |
| 137.0 | 24.1 | 138.67 | 1139.9 | 301.7 | 838.2 | |
| 147.0 | 22.8 | 131.44 | 1159.3 | 323.7 | 835.6 | |
| 157.0 | 21.7 | 125.02 | 1177.6 | 345.7 | 831.9 | |
| 167.0 | 20.7 | 119.27 | 1195.1 | 367.7 | 827.4 | |
| 177.0 | 19.8 | 114.10 | 1211.8 | 389.8 | 822.0 | |
| 187.0 | 19.0 | 109.42 | 1227.7 | 411.8 | 815.9 | |
| 197.0 | 18.3 | 105.15 | 1242.9 | 433.8 | 809.1 | |
| 207.0 | 17.6 | 101.25 | 1257.6 | 455.8 | 801.8 | |
| 217.0 | 17.0 | 97.67 | 1271.7 | 477.8 | 793.8 | |
| 227.0 | 16.4 | 94.36 | 1285.2 | 499.9 | 785.4 | |
| 237.0 | 15.9 | 91.31 | 1298.4 | 521.9 | 776.5 | |

| | | Modi | ied Ratio | nal Method | | |
|-------|---------------|------------|--------------|------------|---------|---|
| Pro | ject Name : | Spadian EA | | ***** | | |
| | | Finch West | Parking Lot | | | |
| F | Project No. : | 33015347 | | | | |
| | | | | | | |
| | Area = | 2.3 | ha | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 2.07 | | | | |
| T | 1c = | 7.0 | min | | | |
| Time | Increment = | 10.0 | 11111 17. | NT | 100 | 1 |
| Re. | lease Rate = | 48.5 | 1/S | North York | TUOyr | |
| Ma | ax.Storage = | 1013 | m3 | a= | 1334 | |
| | | | | b≕ | 2.00 | |
| | | | | c= | 0.771 | |
| Time | Rainfall | Storm | Runoff | Released | Storage | l |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| 7.0 | 245.2 | 1410.75 | 592.5 | 20.4 | 572.1 | |
| 17.0 | 137.8 | 792.96 | 808.8 | 49.5 | 759.4 | |
| 27.0 | 99.5 | 572.35 | 927.2 | 78.6 | 848.6 | |
| 37.0 | 79.1 | 455.47 | 1011.1 | 107.7 | 903.5 | |
| 47.0 | 66.4 | 381.97 | 1077.2 | 136.8 | 940.4 | |
| 57.0 | 57.5 | 331.01 | 1132,1 | 165.9 | 966.2 | |
| 67.0 | 51.0 | 293.37 | 1179.4 | 195.0 | 984.4 | |
| 77.0 | 45.9 | 264.30 | 1221.1 | 224.1 | 997.0 | |
| 87.0 | 41.9 | 241.10 | 1258.5 | 253.2 | 1005.4 | |
| 97.0 | 38.6 | 222.09 | 1292.6 | 282.3 | 1010.3 | |
| 107.0 | 35.0 | 206 21 | 1373.0 | 311 4 | 1012.5 | 1 |
| 1170 | 33 5 | 102 72 | 1323.3 | 340.5 | 1012.5 | |
| 127.0 | 31.5 | 181.09 | 1379.9 | 369.6 | 1010.4 | |
| 137.0 | 29.7 | 170.96 | 1405.3 | 398.7 | 1006.7 | |
| 147.0 | 28.2 | 162.05 | 1429.3 | 427.8 | 1001.5 | |
| 157.0 | 26.8 | 154.13 | 1451.9 | 456.9 | 995.1 | |
| 167.0 | 25.6 | 147.05 | 1473.5 | 486.0 | 987.5 | |
| 177.0 | 24.4 | 140.68 | 1494.0 | 515.1 | 978.9 | |
| 187.0 | 23.4 | 134.90 | 1513.6 | 544.2 | 969.4 | |
| 197.0 | 22.5 | 129.64 | 1532.4 | 573.3 | 959.1 | |
| 207.0 | 21.7 | 124.84 | 1550.5 | 602.4 | 948.1 | |
| 217.0 | 20.9 | 120.42 | 1567.8 | 631.5 | 936.4 | |
| 227.0 | 20.2 | 116.34 | 1584.6 | 660.6 | 924.0 | |

| D. | cient Nome | Castin DA | ultu Kath | Juai Methou | |
|-------|---------------|------------|-------------|-----------------|---------|
| Pr | oject ivame : | Spadian EA | n | <u>` 1 1 00</u> | |
| | Project No | 33015347 | Passenger p | ack-up drop-off | |
| 1 | 110jeet 140 | 155015547 | | | |
| | Area = | 0.3 | lha | | |
| | "C" = | 0.9 | | | |
| | AC= | 0.27 | | | |
| | Tc = | 7.0 | min | | |
| Time | Increment = | 10.0 | min | | |
| Re | lease Rate = | 2.6 | 1/s | North York | 2.vr |
| M | ax.Storage = | 61 | lm3 | a= | 652.8 |
| | U | 1 | <u>1</u> | h- | 4.00 |
| | | | | 6= 6= | 0.786 |
| | | | | | |
| Time | Rainfall | Storm | Runoff | Released | Storage |
| | Intensity | Runoff | Volume | Volume | Volume |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) |
| 7.0 | 99.1 | 74.41 | 31.3 | 1.1 | 30.2 |
| 17.0 | 59.6 | 44,76 | 45.7 | 2.7 | 43.0 |
| 27.0 | 43.9 | 32.96 | 53.4 | 4.2 | 49.2 |
| 37.0 | 35.2 | 26.46 | 58.7 | 5.9 | 52.0 |
| 47.0 | 20.7 | 20,40 | 50.7 | 3.8 | 55.0 |
| 57.0 | 29.7 | 10.26 | 02.8 | 7.3 | 55.5 |
| 67.0 | 23.6 | 19.30 | 66.2 | 8.9 | 57.3 |
| 07.0 | 22.9 | 17.18 | 69.1 | 10.5 | 58.6 |
| 77.0 | 20.6 | 15.49 | 71.6 | 12.0 | 59.6 |
| 87.0 | 18.8 | 14.14 | 73.8 | 13.6 | 60.2 |
| 97.0 | 17.4 | 13.03 | 75.8 | 15.1 | 60.7 |
| 107.0 | 16.1 | 12.09 | 77.6 | 16.7 | 61.0 |
| 117.0 | 15.1 | 11.30 | 79.3 | 18.3 | 61.1 |
| 127.0 | 14.1 | 10.62 | 80.9 | 19.8 | 61.1 |
| 137.0 | 13.4 | 10.02 | 82.4 | 21.4 | 61.0 |
| 147.0 | 12.7 | 9.50 | 83.7 | 22.9 | 60.8 |
| 157.0 | 12.0 | 9.03 | 85.1 | 24.5 | 60.6 |
| 107.0 | 11.5 | 8.61 | 86.3 | 26.1 | 60.2 |
| 1/7.0 | 11.0 | 8.23 | 87.5 | 27.6 | 59.8 |
| 107.0 | 10.5 | 7.89 | 88.6 | 29.2 | 59.4 |
| 207.0 | 07 | 7.38 | 89.6 | 30.7 | 58.9 |
| 217.0 | 9.4 | 7.50 | 90.7 | 32.3 | 57.0 |
| 227.0 | 9,1 | 6.80 | 92.6 | 35.4 | 57.5 |
| 237.0 | 00 | 6.50 | 02.5 | 27.0 | 51.4 |

| | | nal Method | ied Ratio | Modif | | |
|-----|---------|----------------|--------------|---------------|--------------|-------|
| | | | | Spadian EA | ject Name : | Pro |
| | | ck-up drop-off | Passenger pi | Finch West- | | |
| | | | | 33015347 | roject No. : | P |
| | | | | 0.0 | | |
| | | | na | 0.5 | Area = | |
| | | | | 0.9 | -C = | |
| | | | l | 0.27 | AC= | |
| | | | min min | 10.0 | IC = | Time |
| ٦ | 5 | North Vork | | 2.0 | ancientent - | Del |
| 4 | Jyi | | | - 3,0 - 90 | ease Rate = | Kei |
| | 840.7 | a= | mo | 80 | ix.Storage = | Ma |
| | 3:00 | D= | | | | |
| | 0.779 | c= | | | | |
| ٦ | Storage | Released | Runoff | Storm | Rainfall | Time |
| | Volume | Volume | Volume | Runoff | Intensity | |
| | (m3) | (m3) | (m3) | (l/s) | (mm/hr) | (min) |
| | 42.5 | 1.6 | 44,1 | 104.97 | 139.8 | 7.0 |
| | 58.5 | 3.9 | 62.4 | 61.17 | 81.5 | 17.0 |
| | 66.1 | 6.2 | 72.3 | 44.60 | 59.4 | 27.0 |
| | 70.7 | 8.4 | 79.1 | 35.65 | 47.5 | 37.0 |
| | 73.8 | 10.7 | 84.5 | 29.96 | 39.9 | 47.0 |
| | 75.9 | 13.0 | 88.9 | 25,99 | 34.6 | 57.0 |
| | 77.4 | 15.3 | 92.7 | 23.05 | 30.7 | 67.0 |
| | 78.4 | 17.6 | 96.0 | 20.78 | 27.7 | 77.0 |
| | 79,1 | 19.8 | 98.9 | 18.95 | 25.3 | 87.0 |
| | 79.5 | 22.1 | 101.6 | 17,46 | 23.3 | 97.0 |
| <<< | 79.7 | 24.4 | 104.1 | 16.21 | 21.6 | 107.0 |
| | 79.7 | 26.7 | 106.3 | 15.15 | 20.2 | 117.0 |
| | 79.5 | 29.0 | 108.5 | 14.23 | 19.0 | 127.0 |
| | 79.2 | 31.2 | 110.4 | 13.43 | 17.9 | 137.0 |
| | 78.8 | 33.5 | 112.3 | 12.73 | 17.0 | 147.0 |
| | 78.3 | 35.8 | 114.0 | 12.11 | 16.1 | 157.0 |
| | 77.6 | 38.1 | 115.7 | 11.55 | 15.4 | 167.0 |
| | 76.9 | 40.4 | 117.3 | 11.05 | 14.7 | 177.0 |
| | 76.2 | 42.6 | 118.8 | 10.59 | 14.1 | 187.0 |
| | 75.4 | 44.9 | 120.3 | 10.18 | 13.6 | 197.0 |
| 8 | 74.5 | 47.2 | 121.7 | 9.80 | 13.1 | 207.0 |
| | 73.5 | 49.5 | 123.0 | 9.45 | 12.6 | 217.0 |
| | 72.5 | 51.8 | 124.3 | 9.13 | 12.2 | 227.0 |

| | | nal Method | fied Ratio | Modi | | |
|---|---------|----------------|--------------|------------|---------------|-------|
|] | | | | Spadian EA | oject Name : | Pro |
|] | | ck-up drop-off | Passenger pi | Finch West | | |
|] | | | | 33015347 | Project No. : |] |
| | | | ha | 0.3 | Area = | |
| | | | | 0.9 | "C" = | |
| | | | | 0.27 | AC= | |
| | | | min | 7.0 | Tc = | |
| | | | min | 10.0 | Increment = | Time |
| 1 | 25yr | North York | 1/s | 5.8 | lease Rate = | Re |
| İ | 1082 | a= | m3 | 103 | ax.Storage = | M |
| | 2.00 | b= | 2 | 5 5 | L | |
|] | 0.771 | c= | | | | |
| 1 | Storoza | Released | Runoff | Storm | Rainfall | Time |
| | Storage | Reitaseu | Runon | Broth | Namiai | Thic |
| | Volume | Volume | Volume | Runoff | Intensity | |
| 1 | (m3) | (m3) | (m3) | (l/s) | (mm/hr) | (min) |
| | 60.2 | 2.4 | 62.7 | 149.25 | 198.8 | 7.0 |
| | 79.7 | 5.9 | 85.6 | 83.89 | 111.8 | 17.0 |
| | 88.7 | 9.4 | 98.1 | 60.55 | 80.7 | 27.0 |
| | 94.1 | 12.9 | 107.0 | 48.19 | 64.2 | 37.0 |
| | 97.6 | 16.4 | 114.0 | 40.41 | 53.8 | 47.0 |
| | 99.9 | 19.8 | 119.8 | 35.02 | 46.7 | 57.0 |
| | 101.5 | 23.3 | 124.8 | 31.04 | 41.3 | 67.0 |
| | 102.4 | 26.8 | 129.2 | 27.96 | 37.3 | 77.0 |
| | 102.9 | 30.3 | 133.1 | 25.51 | 34.0 | 87.0 |
| < | 103.0 | 33.8 | 136.7 | 23.50 | 31.3 | 97.0 |
| | 102.8 | 37.2 | 140.1 | 21.82 | 29.1 | 107.0 |
| | 102.4 | 40.7 | 143.1 | 20.39 | 27.2 | 117.0 |
| | 101.8 | 44.2 | 146.0 | 19.16 | 25.5 | 127.0 |
| | 101.0 | 47.7 | 148.7 | 18.09 | 24.1 | 137.0 |
| | 100.1 | 51.2 | 151.2 | 17.14 | 22.8 | 147.0 |
| | 99.0 | 54.6 | 153.6 | 16.31 | 21.7 | 157.0 |
| | 97.8 | 58.1 | 155.9 | 15.56 | 20.7 | 167.0 |
| | 96.5 | 61.6 | 158,1 | 14.88 | 19.8 | 177.0 |
| | 95.1 | 65.1 | 160.1 | 14.27 | 19.0 | 187.0 |
| | 93.6 | 68.6 | 162.1 | 13.72 | 18.3 | 197.0 |
| | 92.0 | 72.0 | 164.0 | 13.21 | 17.6 | 207.0 |
| | 90.4 | 75.5 | 165.9 | 12.74 | 17.0 | 217.0 |
| | 88.6 | /9.0 | 107.0 | 12.31 | 10.4 | 227.0 |



| | | Modi | fied Ratio | nal Method | | |
|------------|---------------|------------|------------|------------------|---------------|---|
| Pr | oject Name : | Spadian EA | | | | |
| | | Finch West | Bus Termin | al / Roads / Sta | tion Building | |
| | Project No. : | 33015347 | | | | |
| | | | ח. | | | |
| | Area = | 1.2 | ha | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 1.08 | | | | |
| Time e | Tc = | 7.0 | min | | | |
| Time D- | Increment = | 10.0 | min | | | 1 |
| Re | lease Kate = | 9.1 | 1/S | North York | 2yr | |
| M | ax.Storage = | 255 | m3 | a | = 652.8 | |
| | | | | b | = 4.00 | |
| | | | | C | =0.786 | I |
| Time | D-i-C-II | | D 62 | <u> </u> | T | 1 |
| THIE | Kainiali | Storm | Runoff | Released | Storage | |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| 7.0 | 99.1 | 297.66 | 125.0 | 3.8 | 121.2 | |
| 17.0 | 59.6 | 179.05 | 182.6 | 9.3 | 173.4 | |
| 27.0 | 43.9 | 131.84 | 213.6 | 14.7 | 198.8 | |
| 37.0 | 35.2 | 105.83 | 234.9 | 20.2 | 214.7 | |
| 47.0 | 29.7 | 89.15 | 251.4 | 25.7 | _ 225.7 | |
| 57.0 | 25.8 | 77.44 | 264.9 | 31.1 | 233.7 | |
| 67.0 | 22.9 | 68.73 | 276.3 | 36.6 | 239.7 | |
| 77.0 | 20.6 | 61.97 | 286.3 | 42.0 | 244,3 | |
| 87.0 | 18.8 | 56.55 | 295.2 | 47.5 | 247.7 | ĺ |
| 97.0 | 17.4 | 52.10 | 303.2 | 53.0 | 250,3 | |
| 107.0 | 16.1 | 48.38 | 310.6 | 58.4 | 252.1 | |
| 117.0 | 15.1 | 45.20 | 317.3 | 63.9 | 253.5 | |
| 127.0 | 14.1 | 42.47 | 323.6 | 69.3 | 254.3 | |
| 137.0 | 13.4 | 40.08 | 329.5 | 74.8 | 254.7 | |
| 147.0 | 12,7 | 37.98 | 335.0 | 80.3 | 254.7 | < |
| 157.0 | 12.0 | 36.11 | 340.2 | 85.7 | 254.5 | |
| 167.0 | 11.5 | 34.44 | 345.1 | 91.2 | 253.9 | |
| 177.0 | 11.0 | 32.94 | 349.8 | 96.6 | 253.2 | |
| 187.0 | 10.5 | 31.58 | 354.3 | 102.1 | 252.2 | |
| 197.0 | 10.1 | 30.33 | 358.6 | 107.6 | 251.0 | |
| 207.0 | 9.7 | 29.20 | 362.6 | 113.0 | 249.6 | |
| 217.0 | 9.4 | 28.16 | 366.6 | 118.5 | 248.1 | |
| 441.0 | 7.1 | 27.19 | 370.4 | 123.9 | 246.4 | |

| | | Modi | fied Ratio | nal Method | | |
|-------|---------------|----------------|-------------|--------------------|-------------|-----|
| Pro | oject Name : | Spadian EA | | | |] |
| | | Finch West | Bus Termina | al / Roads / Stati | on Building |] |
|] | Project No. : | 33015347 | | | |] |
| | | | 7 | | | |
| | Area = | 1.2 | ha | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 1.08 | | | | |
| | Tc = | 7.0 | min | | | |
| Time | Increment = | 10.0 | min | P | | 5 |
| Re | lease Rate = | 13.5 | l/s | North York | 5yr | |
| Ma | ax.Storage = | 331 | m3 | a= | 840.7 | |
| | | | | b= | 3.00 | |
| | | | | c= | 0.779 | |
| | | r | | · | P | ล |
| Time | Rainfall | Storm | Runoff | Released | Storage | |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (1/s) | (m3) | (m3) | (m3) | |
| 7.0 | 139.8 | 419.86 | 176.3 | 5.7 | 170.7 | |
| 17.0 | 81.5 | 244.68 | 249.6 | 13.8 | 235.8 | |
| 27.0 | 59.4 | 178.42 | 289.0 | 21.9 | 267.2 | |
| 37.0 | 47.5 | 142.60 | 316.6 | 30.0 | 286.6 | |
| 47.0 | 39.9 | 119.84 | 338.0 | 38.1 | 299.9 | |
| 57.0 | 34.6 | 103.98 | 355.6 | 46.2 | 309.4 | |
| 67.0 | 30.7 | 92,21 | 370.7 | 54.3 | 316.4 | |
| 77.0 | 27.7 | 83.10 | 383.0 | 62.4 | 321.6 | |
| 87.0 | 25.2 | 75.01 | 205.9 | 70.5 | 321.0 | |
| 07.0 | 22,3 | 75.01 | 393.0 | 70.3 | 325.3 | |
| 107.0 | 23.3 | 09.84 | 400.3 | /8.0 | 327.9 | |
| 107.0 | 21.0 | 64.84 | 416.3 | 86.7 | 329.6 | |
| 127.0 | 20.2 | 60.59 56.02 | 425.4 | 94.8 | 330.6 | |
| 137.0 | 19.0 | 53 74 | 455.8 | 102.9 | 330.9 | <<< |
| 147.0 | 17.0 | 50.93 | 449.2 | 1191 | 330.0 | |
| 157.0 | 16.1 | 48.43 | 456.2 | 127.2 | 329.0 | |
| 167.0 | 15.4 | 46.19 | 462.9 | 135.3 | 327.6 | |
| 177.0 | 14.7 | 44.18 | 469.2 | 143.4 | 325.9 | |
| 187.0 | 14.1 | 42.36 | 475.3 | 151.5 | 323.8 | |
| 197.0 | 13.6 | 40.70 | 481.1 | 159.6 | 321.5 | |
| 207.0 | 13.1 | 39.18 | 486.7 | -167.7 | 319.0 | |
| 217.0 | 12.6 | 37.79 | 492.0 | 175.8 | 316.2 | |
| 227.0 | 12.2 | 36.50 | 497.2 | 183.9 | 313.3 | |
| 237.0 | 11.8 | 35.31 | 502.1 | 192.0 | 310.2 | |

| | | Modi | fied Ratio | nal Method | | |
|-------|---------------|------------|-------------|--------------------|-------------|------|
| Pro | oject Name : | Spadian EA | | | | |
| | | Finch West | Bus Termina | al / Roads / Stati | on Building | |
| I | Project No. : | 33015347 | | | | |
| | Area = | 1.2 | ha | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 1.08 | | | | |
| | Tc = | 7.0 | min | | | |
| Time | Increment = | 10.0 | min | | | |
| Re | lease Rate = | 20.5 | l/s | North York | 25yr |] |
| Ma | x.Storage = | 429 | m3 | a= | 1082 | |
| | U | 1 <u></u> | 1 | h= | 2.00 | |
| | | | | c= | 0.771 | |
| | | | | | | 1 |
| Time | Rainfall | Storm | Runoff | Released | Storage | 1 |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (1/s) | (m3) | (m3) | (m3) | |
| 7.0 | 198.8 | 597.00 | 250.7 | 8.6 | 242.1 | |
| 17.0 | 111.8 | 335.57 | 342.3 | 20.9 | 321.4 | |
| 27.0 | 80.7 | 242.21 | 392.4 | 33.2 | 359.2 | |
| 37.0 | 64.2 | 192.75 | 427.9 | 45.5 | 382.4 | |
| 47.0 | 53.8 | 161.64 | 455.8 | 57.9 | 302.4 | |
| 57.0 | 46.7 | 140.08 | 479.1 | 70.1 | 409.0 | |
| 67.0 | 41.3 | 124.15 | 499.1 | 82.4 | 416.7 | |
| 77.0 | 37 3 | 111.85 | 5167 | 04.7 | 422.0 | |
| 87.0 | 34.0 | 102.03 | 522.6 | 107.0 | 422.0 | |
| 07.0 | 21.2 | 02.00 | 532.0 | 107.0 | 423.0 | |
| 97.0 | 31.3 | 93.99 | 547.0 | 119.3 | 427.7 | |
| 107.0 | 29.1 | 87.26 | 560.2 | 131.6 | 428.6 | <<<< |
| 117.0 | 27.2 | 81.55 | 572.5 | 143.9 | 428.6 | |
| 127.0 | 25.5 | 76.64 | 584.0 | 156.2 | 427.8 | |
| 137.0 | 24,1 | 72.35 | 594.7 | 168.5 | 426.2 | |
| 147.0 | 22.8 | 68.38 | 604.8 | 180.8 | 424.0 | |
| 167.0 | 21.7 | 60.00 | 014.4 | 193.1 | 421.3 | |
| 107.0 | 20.7 | 50.52 | 623.3 | 205.4 | 418.1 | |
| 197.0 | 19.8 | 57.00 | 640.5 | 21/./ | 414.5 | |
| 107.0 | 18.3 | 54.86 | 648.5 | 230.0 | 410.5 | |
| 207.0 | 17.5 | 57.82 | 656 1 | 242.3 | 400.2 | |
| 217.0 | 17.0 | 50.06 | 663.5 | 234.0 | 306.6 | |
| 227.0 | 16.4 | 49.23 | 670.6 | 200.9 | 301 / | |
| | A T | 17.23 | 0.010 | 219.2 | 571.4 | 11 |

| 1999-140 - 1997 - 1998 - | | Modi | fied Ratio | onal Method | | |
|-------------------------------------|---------------|------------|------------|-------------------|--------------|------|
| Pre | oject Name : | Spadian EA | | | x | 1 |
| | | Finch West | Bus Termin | al / Roads / Stat | ion Building | 1 |
|] | Project No. : | 33015347 | | | |] |
| | Area = | 1.2 | ha | | | |
| | "C" = | 0.9 | , inc | | | |
| | AC= | 1.08 | | | | |
| | Tc = | 7.0 | min | | | |
| Time | Increment = | 10.0 | min | | | |
| Re | lease Rate = | 27.1 | 1/s | North York | 100vr | 1 |
| M | ax.Storage = | 517 | m3 | a= | 1334 | 1 |
| | 0 | L | | h= | 2.00 | |
| | | | | 0= c= | 0,771 | |
| | | 2 | -2247 | - | L | บ |
| Time | Rainfall | Storm | Runoff | Released | Storage | |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (1/s) | (m3) | (m3) | (m3) | |
| 7.0 | 245.2 | 736.04 | 309.1 | 11.4 | 297.8 | |
| 17.0 | 137.8 | 413.72 | 422.0 | 27.6 | 394.4 | |
| 27.0 | 99.5 | 298.62 | 483.8 | 43.9 | 439.9 | |
| 37.0 | 79.1 | 237.64 | 527.6 | 60.2 | 467.4 | |
| 47.0 | 66.4 | 199.29 | 562.0 | 76.4 | 485.6 | |
| 57.0 | 57.5 | 172.70 | 590.6 | 92.7 | 498.0 | |
| 67.0 | 51.0 | 153.06 | 615.3 | 108.9 | 506.4 | |
| 77.0 | 45.9 | 137.90 | 637.1 | 125.2 | 511.9 | |
| 87.0 | 41.9 | 125.79 | 656.6 | 141.5 | 515.2 | |
| 97.0 | 38.6 | 115.87 | 674.4 | 157.7 | 516.7 | |
| 107.0 | 35.8 | 107.59 | 690.7 | 174.0 | 516.7 | <<<- |
| 117.0 | 33.5 | 100.55 | 705.9 | 190.2 | 515.6 | |
| 127.0 | 31.5 | 94.48 | 720.0 | 206,5 | 513.5 | |
| 137.0 | 29.7 | 89.20 | 733.2 | 222.8 | 510.5 | |
| 147.0 | 28.2 | 84.55 | 745.7 | 239.0 | 506.7 | |
| 157.0 | 26.8 | 80.42 | 757.5 | 255.3 | 502.2 | |
| 167.0 | 25.6 | 76.72 | 768.8 | 271.5 | 497.2 | |
| 177.0 | 24.4 | 73.40 | 779.5 | 287.8 | 491.7 | |
| 187.0 | 23.4 | 70.38 | 789.7 | 304.1 | 485.6 | |
| 197.0 | 22.5 | 67.64 | 799.5 | 320.3 | 479.2 | |
| 207.0 | 21.7 | 65.13 | 808.9 | 336.6 | 472.4 | |
| 227.0 | 20.9 | 60.70 | 818.0 | 352.8 | 465.2 | |
| 227.0 | 10.6 | 59.72 | 020.7 | 205.1 | 457.0 | |

| Pr | oiect Name - | Snadian EA | | | 2 |
|-------|---------------|-------------|---------------|------------|---------|
| L.J. | oject maine : | York II Sta | tion Building | - | |
| | Project No. : | 33015347 | aon Danonig | | (|
| | | 55015511 | | | |
| | Area = | 0.1 | lha | | |
| | "C" = | 0.9 | | | |
| | AC= | 0.09 | | | |
| | Tc = | 7.0 | min | | |
| Time | Increment = | 5.0 | min | | |
| Re | lease Rate = | 4.2 | 1/s | North York | 2vr |
| М | ax.Storage = | 11 | m3 | 2= | 652.8 |
| | | | 1 | h- | 4.00 |
| | | | | c= | 0.786 |
| | | | | - 1 | |
| Time | Rainfall | Storm | Runoff | Released | Storage |
| | Intensity | Runoff | Volume | Volume | Volume |
| (min) | (mm/hr) | (1/s) | (m3) | (m3) | (m3) |
| 7.0 | 99.1 | 24.80 | 10.4 | 1.8 | 8.7 |
| 12.0 | 73.8 | 18.48 | 13.3 | 3.0 | 10.3 |
| 17.0 | 59.6 | 14.92 | 15.2 | 4.3 | 10.9 |
| 22.0 | 50.4 | 12.62 | 16.7 | 5.5 | 11.1 |
| 27.0 | 43.9 | 10,99 | 17.8 | 6.8 | 11.0 |
| 32.0 | 39.0 | 9.77 | 18.8 | 8.1 | 10.7 |
| 37.0 | 35.2 | 8.82 | 19.6 | 9.3 | 10.3 |
| 42.0 | 32.2 | 8.06 | 20.3 | 10.6 | 9.7 |
| 47.0 | 29.7 | 7.43 | 20.9 | 11.8 | 9.1 |
| 52.0 | 27.6 | 6.90 | 21.5 | 13.1 | 8.4 |
| 57.0 | 25.8 | 6.45 | 22.1 | 14.4 | 7.7 |
| 62.0 | 24.2 | 6.07 | 22.6 | 15.6 | 6.9 |
| 67.0 | 22.9 | 5.73 | 23.0 | 16.9 | 6.1 |
| 72.0 | 21.7 | 5.43 | 23.5 | 18.1 | 5.3 |
| 77.0 | 20.6 | 5.16 | 23.9 | 19.4 | 4.5 |
| 82.0 | 19.7 | 4.93 | 24.2 | 20.7 | 3.6 |
| 87.0 | 18.8 | 4.71 | 24.6 | 21.9 | 2.7 |
| 92.0 | 18.1 | 4.52 | 24.9 | 23.2 | 1.8 |
| 97.0 | 17.4 | 4.34 | 25.3 | 24.4 | 0.8 |
| 102.0 | 16.7 | 4.18 | 25.6 | 25.7 | -0.1 |
| 107.0 | 16.1 | 4.03 | 25.9 | 27.0 | -1.1 |
| 112.0 | 15.6 | 3.89 | 26.2 | 28.2 | -2.1 |
| 117.0 | 15.1 | 3.77 | 26.4 | 29.5 | -3.0 |
| 122.0 | 14.6 | 3.65 | 26.7 | 30.7 | -4.0 |





| | | 2 |
|------------|--------------|------|
| al Method | | |
| | | |
| | | |
| | | |
| | <i>©</i> . | |
| | | |
| | | |
| | | |
| | | |
| | | , |
| North York | 25yr | |
| a= | 1082 | |
| b= | 2.00 | |
| c= | 0.771 | |
| | | 1 |
| Released | Storage | |
| Volume | Volume | |
| (m3) | (m3) | |
| 1.8 | 19.1 | |
| 3.0 | 22.5 | |
| 4.3 | 24.2 | |
| 5.5 | 25.3 | |
| 6.8 | 25.9 | |
| 8.1 | 26.2 | |
| 9.3 | 26.3 | <<<< |
| 10.6 | 26.3 | |
| 11.8 | 26.1 | |
| 13.1 | 25.9 | |
| 14.4 | 25.6 | |
| 15.6 | 25.2 | |
| 16.9 | 24.7 | |
| 18.1 | 24.2 | |
| 19.4 | 23.7 | |
| 20.7 | 23.1 | |
| 21.9 | 22.5 | |
| 23.2 | 21.8 | |
| 24.4 | 21.1 | |
| 23.7 | 20.4 10 7 | |
| 28.2 | 19.7 | |
| 29.5 | 18.2 | |
| 30.7 | 17.5 | |

| | | 19 | | 10 | | |
|-------|--|--|--|--|---|--|
| | | Modi | fied Ratio | nal Method | | |
| Pr | oject Name : | Spadian EA | | | | 1 |
| | | York U Stat | ion Building | 3 | · · · · · · · · · · · · · · · · · · · | 1 |
| | Project No. : | 33015347 | | | |] |
| | 2 | | | | | |
| | Area = | 0.1 | ha | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 0.09 | | | | |
| | Tc = | 7.0 | min | | | |
| Time | Increment = | 5.0 | min | | | a |
| Re | elease Rate = | 4.2 | l/s | North York | 100yr | |
| M | ax.Storage = | 35 | m3 | a= | 1334 | |
| | | | | b= | 2.00 | |
| | | | | c= | 0.771 | |
| | 1 | | | | | n |
| Time | Rainfall | Storm | Runoff | Released | Storage | |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| 7.0 | 245.2 | 61.34 | 25.8 | 1.8 | 24.0 | |
| 12.0 | 174.4 | 43.63 | 31.4 | 3.0 | 28.4 | |
| 17.0 | 137.8 | 34.48 | 35.2 | 4.3 | 30.9 | |
| 22.0 | 115.1 | 28.79 | 38.0 | 5.5 | 32.5 | |
| 27.0 | 99.5 | 24.88 | 40.3 | 6.8 | 33.5 | |
| 32.0 | 88.0 | 22.01 | 42.3 | 8.1 | 34.2 | |
| 37.0 | 79.1 | 19.80 | 44.0 | 9.3 | 34.6 | |
| 42.0 | 72.1 | 18.04 | 45.5 | 10.6 | 34.9 | |
| 47.0 | 66.4 | 16.61 | 46.8 | 11.8 | 35.0 | |
| 52.0 | 61.6 | 15.41 | 48.1 | 13.1 | 35.0 | |
| 57.0 | 57.5 | 14 30 | 49.2 | 14.4 | 34.0 | |
| 62.0 | 54.0 | 13.52 | 50.3 | 15.6 | 34.9 | |
| 67.0 | 51.0 | 12.76 | 51.3 | 16.9 | 34.4 | |
| 72.0 | 48.3 | 12.09 | 52.2 | 18.1 | 34.1 | 8 |
| 77.0 | 45.9 | 11.49 | 53.1 | 19.4 | 33.7 | |
| 82.0 | 43.8 | 10.96 | 53.9 | 20.7 | 33.3 | |
| 87.0 | 41.9 | 10.48 | 54.7 | 21.9 | 32.8 | 10 |
| 92.0 | 40.2 | 10.05 | 55.5 | 23.2 | 32.3 | |
| 97.0 | 38.6 | 9.66 | 56.2 | 24.4 | 31.8 | |
| 102.0 | 37.2 | 9.30 | 56.9 | 25.7 | 31.2 | |
| 107.0 | 35.8 | 8.97 | 57.6 | 27.0 | 30.6 | |
| 112.0 | 34.6 | 8.66 | 58.2 | 28.2 | 30.0 | |
| 117.0 | 33.5 | 8.38 | 58.8 | 29.5 | 29.3 | |
| | Pr Time Re M Time (min) 7.0 12.0 17.0 22.0 27.0 32.0 37.0 42.0 47.0 52.0 57.0 62.0 67.0 52.0 57.0 62.0 67.0 72.0 77.0 82.0 87.0 92.0 97.0 102.0 0 77.0 102.0 0 77.0 102.0 1000 | Project Name : Project No. : Area = "C" = AC= Tc = Time Increment = Release Rate = Max.Storage = Time (mm/hr) 7.0 245.2 12.0 174.4 17.0 137.8 22.0 115.1 27.0 99.5 32.0 88.0 37.0 79.1 42.0 72.1 47.0 66.4 52.0 51.0 77.0 45.9 82.0 31.0 77.0 45.9 82.0 41.9 92.0 40.2 97.0 38.6 102.0 37.2 107.0 35.8 112.0 34.6 117.0 33.5 | Modii $Project Name : Spadian EAYork U StatProject No. : 33015347Area = 0.1"C" = 0.9AC = 0.9Tc = 7.0Time Increment = Release Rate = 4.2Max.Storage = 35Time Increment = Max.Storage = 35Time Increment = 100000000000000000000000000000000000$ | Modified RatioProject Name :Spadian EA York U Station Building Project No. :33015347Area = 0.1 0.9 AC = 0.9 0.9 AC = na rc ="C" = 0.9 AC = 0.9 $AC =$ na Is Time Increment = 5.0 Tc = nin min min minRelease Rate = 4.2 $1/s$ l/s m3Time Increment = 5.0 Max.Storage = 35 Time Increment = 5.0 m3 min m3Time Increment = 5.0 m3 min 7.0 245.2 61.34 (M3) 25.8 12.0 174.4 (Ms) 43.63 (M3) 7.0 245.2 61.34 (M3) 25.8 12.0 174.4 (Ms) 43.63 (M3) 7.0 245.2 61.34 (M3) 25.8 12.0 174.4 (Ms) 43.63 (M3) 21.0 174.4 (Ma) 43.63 (M3) 22.0 115.1 (M3) 28.79 (M4.0) 22.0 115.1 (M3) 28.79 (M4.0) 22.0 115.1 (M3) 28.79 (M4.0) 22.0 61.6 (M3) 15.41 (M4.0) 42.0 (M2.1) 72.1 (M3) 44.0 (M2.2) 42.0 (M2.1) 18.04 (M4.0) 42.0 (M2.1) 18.04 (M3) 45.0 (M3.2) 61.6 (M3) 47.0 (M4.0) 16.61 (M4.8) 57.0 (M3.6) 12.76 (M3.8) 70.0 (M3.8) 12.99 (M3.8)< | Modified Rational Method Spadian EA York U Station Building Project No.: 33015347 Area 0.9 AC= 0.9 AC= 0.09 AC= 0.09 Time Increment = 4.2 Max.Storage = 35 min min Release Rate = 4.2 Max.Storage = 35 min (min) Intensity Runoff Rainfall Storm Runoff Volume (min) (m/hr) 17.0 137.8 34.48 35.2 12.0 174.4 137.8 34.48 32.0 88.0 22.0 115.1 28.79 38.0 32.0 88.0 32.0 88.0 32.0 88.0 32.0 18.04 45.5 10.6 47.0 66.4 | Modified Rational Method Spadian EA York U Station Building Project No. : 33015347 Area = 0.1 0.0 Area = 0.1 na North York 100yr Area = 0.1 nin North York 100yr Max.Storage = 0.1 North York 100yr Max.Storage = 0.1 North York 100yr Max.Storage 133 Na a= 1334 b_{0} Tre = 7.0 min min Tre = 7.0 min Tre = 7.0 min Tre = 1334 Jre = 1334 Quarter to the performant of the perfo |

| T | | Inoria Contraction | neu Kati(| mai method | |
|-------|---------------|--------------------|------------|------------|--|
| Pr | oject Name : | Spadian EA | | | ······································ |
| 5 | Droiget Ma | Steeles East | Parking Lo | t | |
| | Project No. : | 55015547 | | | |
| | Aron - | 5.0 | l. | | |
| | | 0.0 | lia | | |
| | | 1.68 | | | |
| | Tc = | 7.0 | min | | |
| Time | Increment = | 5.0 | min | | |
| Re | lease Rate = | 335.7 | 1/s | North York | 2vr |
| M | ax.Storage = | 450 | m3 | a- | 652.8 |
| | | | Juno - | a- b- | 4.00 |
| | | | | c= | 0.786 |
| | | | | -1 | 0.700 |
| Time | Rainfall | Storm | Runoff | Released | Storage |
| | Intensity | Runoff | Volume | Volume | Volume |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) |
| 7.0 | 99.1 | 1289.84 | 541.7 | 141.0 | 400.7 |
| 12.0 | 73.8 | 960.80 | 691.8 | 241.7 | 450.1 |
| 17.0 | 59.6 | 775.90 | 791.4 | 342.4 | 449.0 |
| 22.0 | 50.4 | 656.00 | 865.9 | 443.1 | 422.8 |
| 27.0 | 43.9 | 571.30 | 925.5 | 543.8 | 381,7 |
| 32.0 | 39.0 | 507.95 | 975.3 | 644.5 | 330.7 |
| 37.0 | 35.2 | 458.59 | 1018.1 | 745.3 | 272.8 |
| 42.0 | 32.2 | 418.93 | 1055.7 | 846.0 | 209.7 |
| 47.0 | 29.7 | 386.30 | 1089.4 | 946.7 | 142.7 |
| 52.0 | 27.6 | 358.92 | 1119.8 | 1047.4 | 72.4 |
| 57.0 | 25.8 | 335.58 | 1147.7 | 1148.1 | -0.4 |
| 62.0 | 24.2 | 315.43 | 1173.4 | 1248.8 | -75.4 |
| 67.0 | 22.9 | 297.84 | 1197.3 | 1349.5 | -152.2 |
| 72.0 | 21.7 | 282.33 | 1219.6 | 1450.2 | -230.6 |
| 77.0 | 20.6 | 268.54 | 1240.6 | 1550.9 | -310.3 |
| 82.0 | 19.7 | 256.19 | 1260.4 | 1651.6 | -391.2 |
| 87.0 | 18.8 | 245.06 | 1279.2 | 1752.4 | -473.2 |
| 92.0 | 18.1 | 234.97 | 1297.0 | 1853.1 | -556.0 |
| 97.0 | 17.4 | 225.77 | 1314.0 | 1953.8 | -639.8 |
| 102.0 | 16.7 | 217.36 | 1330.2 | 2054.5 | -724.2 |
| 107.0 | 16.1 | 209.63 | 1345.8 | 2155.2 | -809.4 |
| 112.0 | 15.6 | 202.49 | 1360.7 | 2255.9 | -895.2 |
| 117.0 | 15.1 | 195.89 | 1375.1 | 2356.6 | -981.5 |

| | | nal Method | fied Ratio | Modi | | |
|---|---------|------------|-------------|--------------|---------------|-------|
| | | | | Spadian EA | oject Name : | Pro |
| | | | Parking Lot | Steeles East | | |
| | | | | 33015347 | Project No. : | I |
| | | | 1 | | | |
| | | | ha | 5.2 | Area = | |
| | | | | 0.9 | "C" = | |
| | | | 3 | 4.68 | AC= | |
| | | | min | 7.0 | Tc = | |
| , | | | min | 5.0 | Increment = | Time |
| 12 - 51 | 5yr | North York | 1/s | 494.4 | lease Rate = | Re |
| | 840.7 | a= | m3 | 599 | ax.Storage = | Ma |
| | 3.00 | b= | | | | |
| | 0.779 | c= | | | | |
| | | | | | | |
| | Storage | Released | Runoff | Storm | Rainfall | Time |
| | Volume | Volume | Volume | Runoff | Intensity | |
| | (m3) | (m3) | (m3) | (1/s) | (mm/hr) | (min) |
| | (III.5) | 207.6 | 764.0 | 1910 41 | 120.9 | 7.0 |
| | 536.5 | 207.0 | 704.2 | 1619.41 | 139.0 | 7.0 |
| <<<< | 599.2 | 356.0 | 955.2 | 1326.65 | 102.0 | 12.0 |
| | 577.2 | 504.3 | 1081.5 | 1060.30 | 81.5 | 17.0 |
| | 523.7 | 652.6 | 1176.3 | 891.12 | 68.5 | 22.0 |
| - | 451.5 | 800.9 | 1252.5 | 773.13 | 59.4 | 27.0 |
| | 367.2 | 949.2 | 1316.4 | 685.65 | 52.7 | 32.0 |
| | 274.2 | 1097.6 | 1371.8 | 617.91 | 47.5 | 37.0 |
| | 174.7 | 1245.9 | 1420.6 | 563,74 | 43.3 | 42.0 |
| | 70.3 | 1394.2 | 1464 5 | 51932 | 30 Q | 47.0 |
| | 38.2 | 1542.5 | 1504.3 | 482.16 | 37.1 | 52.0 |
| | -30.4 | 1600.8 | 15/0.0 | 450.56 | 34.6 | 57.0 |
| | -149.9 | 1090.8 | 1574 0 | 400.00 | 225 | 62.0 |
| | -204.4 | 1039.2 | 1574.8 | 443.34 | 30.7 | 67.0 |
| | -501.2 | 2135.8 | 1635.8 | 378.67 | 29.1 | 72.0 |
| | -620.5 | 2284.1 | 1663.7 | 360.10 | 27.7 | 77.0 |
| | -742.5 | 2432.4 | 1690.0 | 343.49 | 26.4 | 82.0 |
| | -865.8 | 2580.8 | 1714.9 | 328.53 | 25.3 | 87.0 |
| | -990.4 | 2729.1 | 1738.7 | 314.98 | 24.2 | 92.0 |
| The second se | -1116.0 | 2877.4 | 1761.4 | 302.64 | 23.3 | 97.0 |
| | ~1242.6 | 3025.7 | 1783.1 | 291.36 | 22.4 | 102.0 |
| | -1370.1 | 3174.0 | 1803.9 | 280.99 | 21.6 | 107.0 |
| | -1498.4 | 3322.4 | 1824.0 | 271.42 | 20.9 | 112.0 |
| | -1627.4 | 3470.7 | 1843.3 | 262.57 | 20.2 | 117.0 |

| | | Modi | fied Ratio | onal Method | | |
|-------|---------------|--------------|------------|-------------|---------|-----|
| Pro | ject Name : | Spadian EA | | | |] |
| | | Steeles East | Parking Lo | t | 2 | |
| I | Project No. : | 33015347 | | | |] |
| | | | 1. | | | |
| | Area = | 5.2 | na | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 4.68 | | | | |
| m | Tc = | 7.0 | min | | | |
| Time | increment = | 5.0 | min | | | 1 |
| Re | lease Rate = | 690.8 | l/s | North York | 25yr | |
| Ma | ax.Storage = | 828 | m3 | a= | 1082 | 2 |
| | | | | - b= | 2.00 | |
| | | | | c= | 0.771 | |
| Time | Rainfall | Storm | Rupoff | Released | Storage | 1 |
| THIC | Kannan | Storm | Runon | Released | Siciage | |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| 7.0 | 198.8 | 2587.00 | 1086.5 | 290.1 | 796.4 | |
| 12.0 | 141.4 | 1840.15 | 1324.9 | 497.4 | 827.5 | <<< |
| 17.0 | 111.8 | 1454.12 | 1483.2 | 704.6 | 778.6 | |
| 22.0 | 93.3 | 1214.44 | 1603.1 | 911.9 | 691.2 | |
| 27.0 | 80.7 | 1049.56 | 1700.3 | 1119.1 | 581.2 | 1 |
| 32.0 | 71.4 | 928.43 | 1782.6 | 1326.3 | 456.2 | 1 |
| 37.0 | 64.2 | 835.23 | 1854.2 | 1533.6 | 320.6 | |
| 42.0 | 58.5 | 761.05 | 1917.9 | 1740.8 | 177.0 | |
| 47.0 | 53.8 | 700.45 | 1975.3 | 1948.1 | 27.2 | |
| 52.0 | 50.0 | 649.89 | 2027.7 | 2155.3 | -127.6 | |
| 57.0 | 46.7 | 607.00 | 2076.0 | 2362.5 | -286.6 | |
| 62.0 | 43.8 | 570.10 | 2120.8 | 2569.8 | -449.0 | |
| 67.0 | 41.3 | 537.98 | 2162.7 | 2777.0 | -614.3 | |
| 72.0 | 39.2 | 509.73 | 2202.0 | 2984.3 | -782.2 | |
| 77.0 | 37.3 | 484.67 | 2239.2 | 3191.5 | -952.3 | |
| 82.0 | 35.5 | 462.27 | 2274.4 | 3398.7 | -1124.4 | |
| 87.0 | 34.0 | 442.12 | 2307.9 | 3606.0 | -1298.1 | |
| 92.0 | 32.6 | 423.87 | 2339.8 | 3813.2 | -1473.4 | |
| 97.0 | 31.3 | 407.27 | 2370.3 | 4020.5 | -1650.1 | |
| 102.0 | 30.1 | 392.09 | 2399.6 | 4227.7 | -1828.1 | |
| 107.0 | 29.1 | 378.15 | 2427.7 | 4434.9 | -2007.2 | |
| 112.0 | 28.1 | 365.30 | 2454.8 | 4642.2 | -2187.4 | |
| 117.0 | 27.2 | 353.40 | 2480.9 | 4849.4 | -2368.5 | |
| 122.0 | 26.3 | 342.37 | 2506.1 | 5056.7 | -2550.5 | |

| | | nal Method | fied Ratio | Modi | 01 | |
|-----|---------|------------|------------|--------------|---------------|----------|
| | | 2 | | Spadian EA | oject Name : | Pro |
| | | | Parking Lo | Steeles East | | |
| | | | ····· | 33015347 | Project No. : | 1 |
| | | | 1 | | | |
| | | | ha | 5.2 | Area = | |
| | | | с. | 0.9 | "C" = | |
| | | | | 4.68 | AC= | |
| | | | min | 7.0 | Tc = | 10000-01 |
| n | | | min | 5.0 | Increment = | Time |
| | 100yr | North York | 1/s | 851.7 | lease Rate = | Re |
| | 1334 | a= | m3 | 1020 | ax.Storage = | Ma |
| | 2.00 | b= | | | | |
| | 0.771 | c= | | | | |
| 3 | | | | | | |
| | Storage | Released | Runoff | Storm | Rainfall | Time |
| | Volume | Volume | Volume | Runoff | Intensity | |
| | (m3) | (m3) | (m3) | (1/s) | (mm/hr) | (min) |
| | 981.9 | 357.7 | 1339.6 | 3189.52 | 245.2 | 7.0 |
| <<< | 1020.3 | 613.2 | 1633.5 | 2268.72 | 174.4 | 12.0 |
| | 959.9 | 868.7 | 1828.6 | 1792.78 | 137.8 | 17.0 |
| | 852.2 | 1124.2 | 1976.4 | 1497.28 | 115.1 | 22.0 |
| | 716.5 | 1379.8 | 2096.3 | 1294.01 | 99.5 | 27.0 |
| | 562.5 | 1635.3 | 2197.7 | 1144.66 | 88.0 | 32.0 |
| | 395.3 | 1890.8 | 2286.1 | 1029.76 | 79.1 | 37.0 |
| | 218.2 | 2146.3 | 2364.5 | 938.31 | 72.1 | 42.0 |
| | 33.5 | 2401.8 | 2435.3 | 863.59 | 66.4 | 47.0 |
| | -157.4 | 2657.3 | 2499 9 | 801.26 | 61.6 | 52.0 |
| | -353.4 | 2912.8 | 2559.4 | 748 38 | 57.5 | 57.0 |
| | -553.6 | 3168.3 | 2614.7 | 702.88 | 54.0 | 62.0 |
| | -757.5 | 3423.8 | 2666.4 | 663.28 | 51.0 | 67.0 |
| | -964.5 | 3679.3 | 2714.9 | 628.45 | 48.3 | 72.0 |
| | -1174.2 | 3934.9 | 2760.7 | 597.55 | 45.9 | 77.0 |
| | -1386.3 | 4190.4 | 2804.1 | 569.94 | 43.8 | 82.0 |
| | -1600.5 | 4445.9 | 2845.4 | 545.09 | 41.9 | 87.0 |
| | -1816.7 | 4701.4 | 2884.7 | 522.59 | 40.2 | 92.0 |
| | -2034.5 | 4956.9 | 2922.4 | 502.12 | 38.6 | 97.0 |
| | -2253.9 | 5212.4 | 2958.5 | 483.41 | 37.2 | 102.0 |
| | -2474.8 | 5467.9 | 2993.1 | 466.22 | 35.8 | 107.0 |
| | -2696.9 | 5723.4 | 3026.5 | 450.37 | 34.6 | 112.0 |
| | -2920.2 | 5978.9 | 3058.7 | 435.71 | 33.5 | 117.0 |

| I | | | Modif | ied Ratio | nal Method | | |
|------|-------|---------------|--------------|---------------|------------|---------|----------|
| | Pro | ject Name : | Spadian EA | | | | |
| | | | Steeles West | t Parking Lot | | | |
| | F | Project No. : | 33015347 | | | | |
| 1 | | | | | | | |
| | | Area = | 4.9 | ha | | | |
| | | "C" = | 0.9 | с; | | | |
| | | AC= | 4.41 | 5 | | | |
| | | Tc = | 7.0 | min | | | |
| | Time | Increment = | 5.0 | min | | | |
| | Re | lease Rate = | 335.2 | l/s | North York | 2yr | |
| | Ma | x.Storage = | 411 | m3 | a= | 652.8 | |
| | | | | | b= | 4.00 | |
| | | | | | c= | 0.786 | |
| | | | | | | | |
| ĺ | Time | Rainfall | Storm | Runoff | Released | Storage | |
| | | Intensity | Runoff | Volume | Volume | Volume | |
| 1 | (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| | 7.0 | 99.1 | 1215.43 | 510.5 | 140.8 | 369.7 | |
| | 12.0 | 73.8 | 905.37 | 651.9 | 241.3 | 410.5 | <<<< |
| | 17.0 | 59.6 | 731.14 | 745.8 | 341.9 | 403.9 | |
| | 22.0 | 50.4 | 618.15 | 816.0 | 442.5 | 373.5 | |
| | 27.0 | 43.9 | 538.34 | 872.1 | 543.0 | 329.1 | a a |
| | 32.0 | 39.0 | 478.64 | 919.0 | 643.6 | 275.4 | |
| | 37.0 | 35.2 | 432.13 | 959.3 | 744.1 | 215.2 | |
| | 42.0 | 32.2 | 394,76 | 994.8 | 844.7 | 150.1 | |
| | 47.0 | 29.7 | 364.01 | 1026.5 | 945,3 | 81.2 | |
| 2 | 52.0 | 27.6 | 338.21 | 1055.2 | 1045.8 | 9,4 | |
| - | 57.0 | 25.8 | 316.22 | 1081.5 | 1146.4 | -64.9 | |
| | 62.0 | 24.2 | 297.24 | 1105.7 | 1246.9 | -141.2 | |
| | 67.0 | 22.9 | 280.66 | 1128.2 | 1347.5 | -219.3 | |
| | 72.0 | 21.7 | 266.04 | 1149.3 | 1448.1 | -298.8 | |
| | 77.0 | 20.6 | 253.04 | 1169.1 | 1548.6 | -379.6 | |
| H 22 | 82.0 | 19.7 | 241.41 | 1187.7 | 1649.2 | -461.5 | |
| | 87.0 | 18.8 | 230.92 | 1205.4 | 1749.7 | -544.4 | |
| | 92.0 | 18.1 | 221.41 | 1222.2 | 1850.3 | -628.1 | |
| | 97.0 | 17.4 | 212.75 | 1238.2 | 1950.9 | -712.7 | |
| | 102.0 | 16.7 | 204.82 | 1253.5 | 2051.4 | -797.9 | |
| | 107.0 | 16.1 | 197.53 | 1268.2 | 2152.0 | -883.8 | |
| | 112.0 | 15.0 | 190.81 | 1282.2 | 2454.5 | -970.3 | |
| | 122.0 | 13.1 | 178.80 | 1308.8 | 2453.7 | -1037.5 | |
| | 122.0 | 1.14.0 | 178.80 | 1.000.0 | L 2+33.1 | -1144.0 | <u> </u> |

| 51 O.17 | | | Modi | fied Ratio | nal Method | ****** | |
|---------|--------------|---------------|-------------|--------------|------------|---------|------------|
| | Pro | oject Name : | Spadian EA | | | |] |
| 3 | | | Steeles Wes | t Parking Lo | t | | |
| |] | Project No. : | 33015347 | | | | |
| | | | _ | 1 | | | |
| | | Area = | 4.9 | ha | | | |
| | | "C" = | 0.9 | | | | |
| | | AC= | 4.41 | | | | |
| | | Tc = | 7.0 | min | | | |
| | Time | Increment = | 5.0 | min | | | 7 1 |
| | Re | lease Rate = | 465.8 | l/s | North York | 5yr | |
| | Ma | ax.Storage = | 565 | m3 | a= | 840.7 | |
| | | | | | b= | 3.00 | |
| | | | | | c= | 0.779 | |
| | | | | | | | สิ |
| | Time | Rainfall | Storm | Runoff | Released | Storage | |
| | | Intensity | Runoff | Volume | Volume | Volume | |
| | (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| | 7.0 | 139.8 | 1714.45 | 720.1 | 195.6 | 524.4 | |
| | 12.0 | 102.0 | 1250.11 | 900.1 | 335.4 | 564.7 | <<<< |
| | 17.0 | 81.5 | 999.13 | 1019.1 | 475.1 | 544.0 | |
| | 22.0 | 68.5 | 839.71 | 1108.4 | 614.9 | 493.6 | |
| | 27.0 | 59.4 | 728.53 | 1180.2 | 754.6 | 425.6 | |
| | 32.0 | 52.7 | 646.09 | 1240.5 | 894.3 | 346.2 | |
| | 37.0 | 47.5 | 582.26 | 1292.6 | 1034.1 | 258.5 | |
| | 42.0 | 43.3 | 531.22 | 1338.7 | 1173.8 | 164.9 | |
| | 42.0 | 20.0 | 490.26 | 1320.0 | 1212.6 | 66.4 | |
| | 47.0 | 37.7 | 407.30 | 1380.0 | 1313.0 | 00.4 | |
| 2 | 52.0 | - 31.1 | 434.34 | 1417.5 | 1455.5 | -33.8 | |
| | 57.0 | 54.0 22.5 | 424.57 | 1452,0 | 1593.0 | -141.0 | |
| | 02.0 67.0 | 30.7 | 398.90 | 1483.9 | 1/32.8 | -248.9 | |
| | 72.0 | 29.1 | 356.82 | 1515.0 | 2012.3 | -338.9 | |
| | 77.0 | 27.7 | 339.33 | 1567.7 | 2152.0 | -584.3 | |
| | 82.0 | 26.4 | 323.67 | 1592.5 | 2291.7 | -699.3 | |
| | 87.0 | 25.3 | 309.58 | 1616.0 | 2431.5 | -815.5 | |
| | 92.0 | 24.2 | 296.81 | 1638.4 | 2571.2 | -932.8 | |
| | 97.0 | 23.3 | 285.18 | 1659.8 | 2711.0 | -1051.2 | |
| | 102.0 | 22.4 | 274.55 | 1680.2 | 2850.7 | -1170.5 | |
| | 107.0 | 21.6 | 264.78 | 1699.9 | 2990.4 | -1290.6 | |
| | 112.0 | 20.9 | 255.76 | 1718.7 | 3130.2 | -1411.4 | |
| | 117.0 | 20.2 | 247.42 | 1736.9 | 3269.9 | -1533.0 | |
| | 122.0 | 19.6 | 239.68 | 1754.5 | 3409.7 | -1655.2 | |

| | | Modi | fied Ratio | nal Method | | |
|---------|---------------|-------------|--------------|------------|-------------------|--------|
| Pr | oject Name : | Spadian EA | | | | 1 |
| | | Steeles Wes | t Parking Lo | t | |] |
| 1 | Project No. : | 33015347 | | | |] |
| | Area = | 4.9 | ha | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 4.41 | | | an an an an ann a | |
| | Tc = | 7.0 | min | | | |
| Time | Increment = | 5.0 | min | | | |
| Re | lease Rate = | 650.9 | 1/s | North York | 25yr | |
| M | ax.Storage = | 780 | m3 | a= | 1082 | |
| | | | 13 | b= | 2.00 | |
| | | | | c= | 0.771 | |
| | | | | 1 | | U U |
| Time | Rainfall | Storm | Runoff | Released | Storage | 1 |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (1/s) | (m3) | (m3) | (m3) | |
| 7.0 | 198.8 | 2437.75 | 1023.9 | 273.4 | 750.5 | |
| 12.0 | 141.4 | 1733.99 | 1248.5 | 468.6 | 779.8 | <<< |
| 17.0 | 111.8 | 1370.22 | 1397.6 | 663.9 | 733.7 | |
| 22.0 | 93.3 | 1144.37 | 1510.6 | 859.2 | 651.4 | |
| 27.0 | 80.7 | 989.01 | 1602.2 | 1054.5 | 547.7 | |
| 32.0 | 71.4 | 874.86 | 1679.7 | 1249 7 | 430.0 | |
| 37.0 | 64.2 | 787.05 | 1747.2 | 1445.0 | 302.2 | |
| 42.0 | 58,5 | 717.15 | 1807.2 | 1640.3 | 166.9 | |
| 47.0 | 53.8 | 660.04 | 1861.3 | 1835.5 | 25.8 | |
| 52.0 | 50.0 | 612 40 | 1910.7 | 2030.8 | -120.1 | |
| 57.0 | 46.7 | 571.98 | 1056.2 | 2000.0 | -120.1 | |
| 62.0 | 43.8 | 537.21 | 1998.4 | 2421.3 | -209.9 | |
| 67.0 | 41,3 | 506.94 | 2037.9 | 2616.6 | -5787 | |
| 72.0 | 39.2 | 480.32 | 2075.0 | 2811.9 | -736.9 | |
| 77.0 | 37.3 | 456.71 | 2110.0 | 3007.2 | -897.2 | |
| 82.0 | 35.5 | 435.60 | 2143.2 | 3202.4 | -1059.3 | |
| 87.0 | 34.0 | 416.61 | 2174.7 | 3397.7 | -1223.0 | |
| 92.0 | 32.6 | 399.42 | 2204.8 | 3593.0 | -1388.2 | |
| 97.0 | 31.3 | 383.77 | 2233.6 | 3788.2 | -1554.7 | |
| 102.0 | 30.1 | 369.47 | 2261.1 | 3983.5 | -1722.4 | |
| 107.0 | 29.1 | 356.33 | 2287.7 | 4178.8 | -1891.1 | |
| 112.0 | 28.1 | 344.22 | 2313.2 | 4374.0 | -2060.9 | |
| 117.0 | 27.2 | 333.02 | 2337.8 | 4569.3 | -2231.6 | |
| 1 4.4.0 | 20.3 | 344.01 | 4.301.3 | 4704.0 | -2403.1 | |

| | | Mod | ified Ratio | nal Method | | |
|-------|---------------|--------------|--------------|---------------|---------|------|
| Pr | roject Name | : Spadian E/ | | Jaar Meetiiou | | ٦ |
| | J | Steeles We | st Parking L | of | | - |
| | Project No. | : 33015347 | | | | - |
| | | | | | | 4 |
| | Area = | 4.9 | ha | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 4.41 | | | | |
| | Tc = | 7.0 | min | | | |
| Time | Increment = | 5.0 | min | | | |
| Re | elease Rate = | 802.5 | l/s | North York | 100yr | 1 |
| М | ax.Storage = | 961 |]m3 | a: | = 1334 | j |
| | | | - | b | = 2.00 | |
| | | 0 | | C= | 0.771 | |
| | | | | | | 0 |
| Time | Rainfall | Storm | Runoff | Released | Storage |] |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| 7.0 | 245.2 | 3005.51 | 1262.3 | 337.1 | 025.2 | |
| 12.0 | 174.4 | 2137.84 | 1539.2 | 577.8 | 061.4 | |
| 17.0 | 137.8 | 1689 35 | 1723 1 | 919.6 | 901.4 | ecc. |
| 22.0 | 115.1 | 1410.00 | 1062.4 | 1050.0 | 904.6 | |
| 27.0 | 00.5 | 1410.90 | 1002.4 | 1059.3 | 803.1 | 10 |
| 27.0 | 99.5 | 1219.30 | 1975.4 | 1300.1 | 675.3 | |
| 52.0 | 88.0 | 1078.62 | 2071.0 | 1540.8 | 530.2 | |
| 37.0 | 79.1 | 970.35 | 2154.2 | 1781.6 | 372.6 | |
| 42.0 | 72.1 | 884.17 | 2228.1 | 2022.3 | 205.8 | |
| 47.0 | 66.4 | 813.76 | 2294.8 | 2263.1 | 31.8 | |
| 52.0 | 61.6 | 755.03 | 2355.7 | 2503.8 | -148.1 | |
| 57.0 | 57.5 | 705.20 | 2411.8 | 2744.6 | -332.8 | |
| 62.0 | 54.0 | 662.33 | 2463.9 | 2985.3 | -521.4 | |
| 67.0 | 51.0 | 625.01 | 2512.5 | 3226.1 | -713.5 | |
| 72.0 | 48.3 | 592.19 | 2558.3 | 3466.8 | -908.5 | |
| 77.0 | 45.9 | 563.08 | 2601.4 | 3707.6 | -1106.1 | |
| 82.0 | 43.8 | 537.06 | 2642.3 | 3948.3 | -1306.0 | |
| 87.0 | 41.9 | 513.64 | 2681.2 | 4189.1 | -1507.8 | |
| 92.0 | 40.2 | 492.44 | 2718.3 | 4429.8 | -1711.5 | |
| 102.0 | 38.0 | 473.16 | 2753.8 | 4670.6 | -1916.8 | |
| 107.0 | 35.8 | 433.52 | 2787.8 | 4911.3 | -2123.5 | × |
| 112.0 | 34.6 | 424 39 | 2820.5 | 5152.1 | -2331.6 | |
| 117.0 | 33.5 | 410.58 | 2882.2 | 5633.6 | -2540.9 | |
| 122.0 | 32.4 | 397.75 | 2911.5 | 5874 3 | -2/31.3 | |

| * | | IVIOD | mea Katio | onal Method | | |
|-------|---------------|------------|--------------|--------------------|---------|------|
| Pr | oject Name : | Spadian EA | | | | - |
| | Decident Ma | Steeles We | st Bus Termi | nal / Station buil | d | 4 |
| | Project No. : | 33013347 | | | | J . |
| | Area = | 2.1 | ha | | | |
| | "C" = | 0.9 | | | | |
| | AC= | 1.89 | 1 | | | |
| | Tc = | 7.0 | min | 15 | | |
| Time | Increment = | 5.0 | min | | | |
| Re | elease Rate = | 143.7 | 1/s | North York | 2vr | 7 |
| М | ax.Storage = | 176 | m3 | a= | 652.8 | |
| | 0 | L | 1 | h= | 4.00 | |
| | | | | c= | 0.786 | |
| | | | | - 1 | | 4. |
| Time | Rainfall | Storm | Runoff | Released | Storage | 1 |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| 7.0 | 99.1 | 520.90 | 218.8 | 60.4 | 158.4 | |
| 12.0 | 73.8 | 388.01 | 279.4 | 103.5 | 175.9 | <<<< |
| 17.0 | 59.6 | 313.34 | 319.6 | 146.6 | 173.0 | |
| 22.0 | 50.4 | 264.92 | 349.7 | 189.7 | 160.0 | |
| 27.0 | 43.9 | 230.72 | 373.8 | 232.8 | 141.0 | |
| 32.0 | 39.0 | 205.13 | 393.9 | 275.9 | 117.9 | |
| 37.0 | 35.2 | 185.20 | 411.1 | 319.0 | 92.1 | |
| 42.0 | 32.2 | 169.18 | 426.3 | 362.1 | 64.2 | |
| 47.0 | 29.7 | 156.00 | 439.9 | 405.2 | 34.7 | |
| 52.0 | 27.6 | 144.95 | 452.2 | 448.3 | 3.9 | |
| 57.0 | 25.8 | 135.52 | 463.5 | 491.5 | -28.0 | |
| 62.0 | 24.2 | 127.39 | 473.9 | 534.6 | -60.7 | |
| 67.0 | 22.9 | 120.28 | 483.5 | 577.7 | -94.1 | |
| 72.0 | 21.7 | 114.02 | 492.6 | 620.8 | -128.2 | |
| 77.0 | 20.6 | 108.45 | 501.0 | 663.9 | -162,9 | |
| 82.0 | 19.7 | 103.46 | 509.0 | 707.0 | -198.0 | |
| 87.0 | 18.8 | 98.96 | 516.6 | 750.1 | -233.5 | |
| 92.0 | 18.1 | 94.89 | 523.8 | 793.2 | -269.4 | |
| 97.0 | 17.4 | 91.18 | 530.7 | 836.3 | -305.7 | |
| 102.0 | 16.7 | 87.78 | 537.2 | 879.4 | -342.2 | |
| 107.0 | 16.1 | 84.66 | 543.5 | 922.6 | -379.1 | |
| 112.0 | 15.6 | 81.78 | 549.5 | 965.7 | -416.1 | |
| 117.0 | 15.1 | 79.11 | 555.3 | 1008.8 | -453.4 | |
| 122.0 | 14.6 | 76.63 | 560.9 | 1051.9 | -491.0 | |

| | | Mod | ified Ratio | onal Method | | |
|-------|---------------------------------------|-------------|--------------|-------------------|---------|----|
| Р | roject Name | : Spadian E | 4 | - | | ٦ |
| | | Steeles We | est Bus Term | inal / Station bu | ild | 1 |
| | Project No. | : 33015347 | | | | |
| | | | - | | 45 P.3 | |
| | Area = | = 2.1 | ha | | | |
| | "C" = | - 0.9 | | | | |
| | AC= | = 1.89 | | | | |
| TT: | Тс = | 7.0 | min | | | |
| Time | = increment = | 5.0 | min | | | |
| R | elease Rate = | 199.6 | 1/s | North York | 5yr |] |
| N | 1ax.Storage = | 242 | Jm3 | a= | = 840.7 |] |
| | | | | b= | = 3.00 |] |
| | | | | C= | =0.779 |] |
| | · · · · · · · · · · · · · · · · · · · | | | | | |
| Time | Rainfall | Storm | Runoff | Released | Storage |] |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (l/s) | (m3) | (m3) | (m3) | |
| 7.0 | 139.8 | 734.76 | 308.6 | 83.8 | 224.8 | i. |
| 12.0 | 102.0 | 535.76 | 385.7 | 143.7 | 242.0 | |
| 17.0 | 81.5 | 428.20 | 436.8 | 203.6 | 233.2 | |
| 22.0 | 68.5 | 359.88 | 475.0 | 263.5 | 255.2 | |
| 27.0 | 59.4 | 312.23 | 505.8 | 322.4 | 102.5 | |
| 32.0 | 52.7 | 276.90 | 531.6 | 323.4 | 182.5 | |
| 37.0 | 47.5 | 040.54 | 551.0 | 363.2 | 148.4 | |
| 31.0 | 47.5 | 249.34 | 554.0 | 443.1 | 110.9 | |
| 42.0 | 43.3 | 227.66 | 573.7 | 503.0 | 70.7 | |
| 47.0 | 39.9 | 209.72 | 591.4 | 562.9 | 28.6 | |
| 52.0 | 37.1 | 194.72 | 607.5 | 622.8 | -15.2 | |
| 57.0 | 34.6 | 181.96 | 622.3 | 682.6 | -60.3 | |
| 62.0 | 32.5 | 170.96 | 636,0 | 742.5 | -106.6 | |
| 67.0 | 30.7 | 161.37 | 648.7 | 802.4 | -153.7 | |
| 72.0 | 29.1 | 152.92 | 660.6 | 862.3 | -201.6 | |
| 77.0 | 27.7 | 145.43 | 671.9 | 922.2 | -250.3 | |
| 82.0 | 26.4 | 138.72 | 682.5 | 982.0 | -299.5 | |
| 87.0 | 25.3 | 132.68 | 692.6 | 1041.9 | -349.3 | |
| 92.0 | 24.2 | 127.20 | 702.2 | 1101.8 | -399.6 | |
| 97.0 | 23.3 | 122.22 | 711.3 | 1161.7 | -450.3 | |
| 102.0 | 22.4 | 117.66 | 720.1 | 1221.6 | -501.5 | |
| 107.0 | 21.6 | 113.48 | 728.5 | 1281.4 | -552.9 | |
| 112.0 | 20.9 | 109.61 | 736.6 | 1341.3 | -604.7 | |
| 117.0 | 20.2 | 100.04 | 744.4 | 1401.2 | -656.8 | |

| | | Modi | fied Ratio | nal Method | ************************************** | |
|------------------------|--------------|-------------|-----------------------------------|--------------|--|---|
| Pr | oject Name : | Spadian EA | | | | 1 |
| | | Steeles Wes | West Bus Terminal / Station build | | | |
| Project No. : 33015347 | | | | ···· | | |
| | , | | Minani | | | 1 |
| | Area = | 2.1 | ha | a 2 | | |
| | "C" = | 0.9 | | | | |
| | AC= | 1.89 | | | | |
| | Tc = | 7.0 | min | | | |
| Time | Increment = | 5.0 | min | | | |
| Re | lease Rate = | 279.0 | 1/s | North York | 25уг | 1 |
| M | ax.Storage = | 334 | m3 | . <u></u> a= | 1082 | |
| | | L | Ŭ. | . h= | 2.00 | |
| | | | | c= | 0.771 | |
| | | | | 5 | 0.771 | |
| Time | Rainfall | Storm | Runoff | Released | Storage | |
| | Intensity | Runoff | Volume | Volume | Volume | |
| (min) | (mm/hr) | (1/s) | (m3) | (m3) | (m3) | |
| 7.0 | 198.8 | 1044 75 | 438.8 | 117.2 | 321.6 | |
| 12.0 | 141.4 | 743 14 | 535.1 | 200.0 | 324.0 | |
| 17.0 | 111.4 | 507.74 | \$00.0 | 200.5 | 334.2 | |
| 22.0 | 00.0 | 367.24 | 399.0 | 284,6 | 314,4 | |
| 22.0 | 93.3 | 490.45 | 647.4 | 368.3 | 279.1 | |
| 27.0 | 80.7 | 423.86 | 686.7 | 452.0 | 234.7 | |
| 32.0 | 71.4 | 374.94 | 719.9 | 535.7 | 184.2 | 1 |
| 37.0 | 64.2 | 337.31 | 748.8 | 619.4 | 129.4 | |
| 42.0 | 58.5 | 307.35 | 774.5 | 703.1 | 71.4 | |
| 47.0 | 53.8 | 282.87 | 797.7 | 786.8 | 10.9 | |
| 52.0 | 50.0 | 262.46 | 818.9 | 870.5 | -51.6 | |
| 57.0 | 46.7 | 245.14 | 838.4 | 954.2 | -115.8 | |
| 62.0 | 43.8 | 230.23 | 856.5 | 1037.0 | 1914 | |
| 67.0 | 41.3 | 217.26 | 873.4 | 1121.6 | -248.2 | |
| 72.0 | 39.2 | 205.85 | 889.3 | 1205 3 | -316.0 | |
| 77.0 | 37.3 | 195.73 | 904.3 | 1289.0 | -384.7 | |
| 82.0 | 35.5 | 186.69 | 918.5 | 1372.7 | -454.2 | |
| 87.0 | 34.0 | 178.55 | 932.0 | 1456.4 | -524.4 | |
| 92.0 | 32.6 | 171.18 | 944.9 | 1540.1 | -595.2 | |
| 97.0 | 31.3 | 164.47 | 957.2 | 1623.8 | -666.5 | |
| 102.0 | 30.1 | 158.34 | 969.1 | 1707.5 | -738.4 | |
| 107.0 | 29.1 | 152.71 | 980.4 | 1791.2 | -810.8 | |
| 112.0 | 28.1 | 147.52 | 991.4 | 1874.9 | -883.5 | |
| 117.0 | 27.2 | 142.72 | 1001.9 | 1958.6 | -956.7 | |
| 122.0 | 26.3 | 138.26 | 1012.1 | 2042.3 | -1030.2 | 1 |

